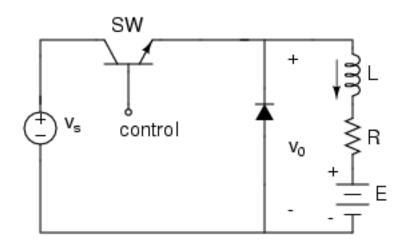
DC-DC Converters (choppers)

- The objective is to convert a fixed DC voltage to a variable DC voltage
- It is possible to step up and step down voltage.

Voltage step down (buck converter)



First, suppose L=0, E=0.

The diode is not needed.

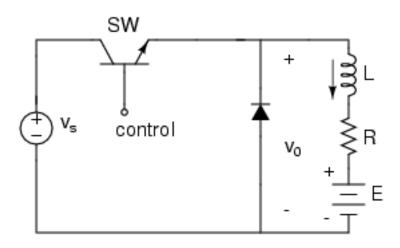
$$V_a = (t_{on}/T)V_s$$

k=t_{on}/T is the duty cycle

$$V_{RMS} = k^{1/2}V_s$$

$$P_{out} = (kV_s^2)/R$$

Step down converter with RL load



$$i_1(t) = I_1 e^{-tR/L} + \frac{V_s - E}{R} (1 - e^{-tR/L}), \quad 0 \le t \le kT$$

Mode 2 (Off): $I_2 = i_1(kT)$, and

$$i_2(t) = I_2 e^{-(t-kT)R/L} + \frac{V_s - E}{R} (1 - e^{-(t-kT)R/L}), \quad kT \le t \le T.$$

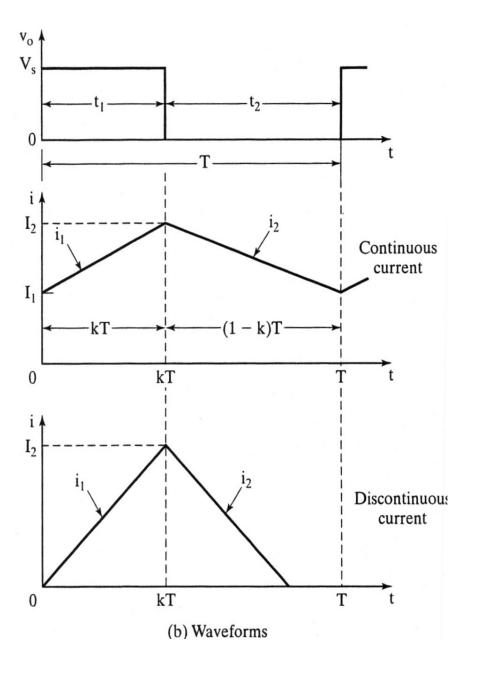
For a steady state current

$$i_{1}(0) = i_{2}(T),$$

$$I_{1} = \frac{V_{s}}{R} \left(\frac{1 - e^{kT(R/L)}}{1 - e^{T(R/L)}} \right) - \frac{E}{R} = \frac{V_{s}}{R} \left(\frac{1 - e^{kz}}{1 - e^{z}} \right) - \frac{E}{R}$$

$$I_{2} = \frac{V_{s}}{R} \left(\frac{1 - e^{-kz}}{1 - e^{-z}} \right) - \frac{E}{R}, \qquad z = T\frac{R}{L},$$

$$\frac{E}{V_e} \le \frac{1 - e^{kz}}{1 - e^z}$$
 for cont. current



Example 5.2

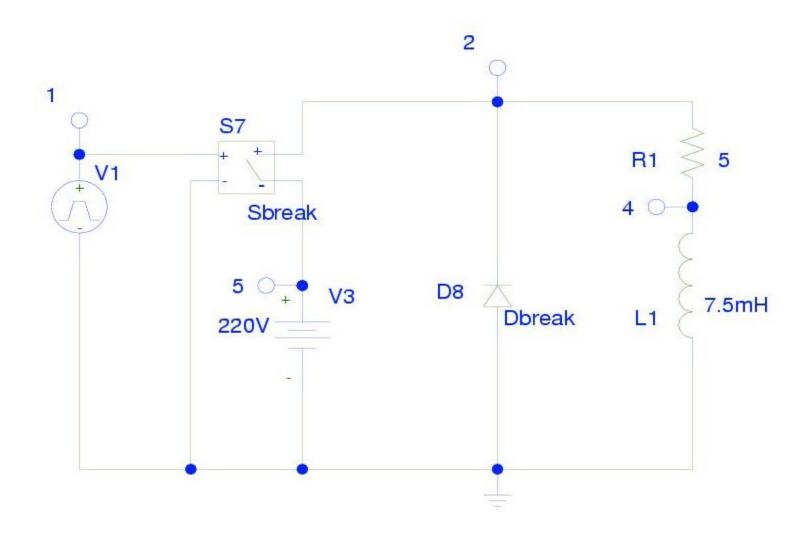
$$I_{a} = \frac{1}{2}(I_{1} + I_{2})$$

$$I_{o} = (I_{1}^{2} + \frac{1}{3}\Delta I^{2} + I_{1}\Delta I)^{1/2}$$

$$I_{s} = kI_{a}$$

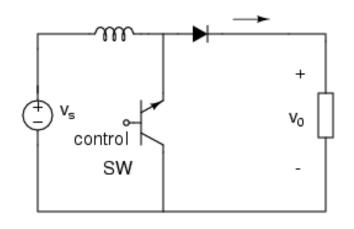
$$I_{R} = \sqrt{k}I_{o}$$

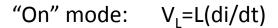
Temperature: 27.0 Date/Time run: 07/17/06 00:05:04 (A) chopperscript.dat (active) 30A 0A □ I(R1) 40A 20A 0A □ -I(V3) 40A 20A SEL>> OA-7ms 8ms 9ms 10ms 5ms 6ms 1ms 2ms 3ms 4ms 0s o I(D) Time Time: 00:10:40 Page 1 Date: July 17, 2006



Pspice schematics Step down dc-dc converter

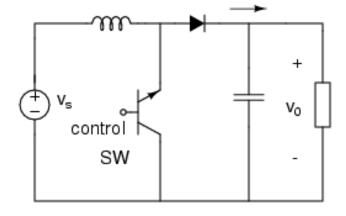
Voltage step up (boost) converter



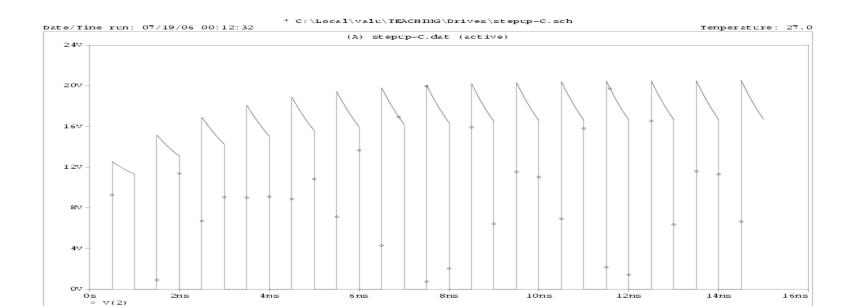


"Off" mode: Assume current decreases at a constant rate. Then

$$V_0 = V_S + V_L$$



To ensure continuous current flow, a capacitor is included.

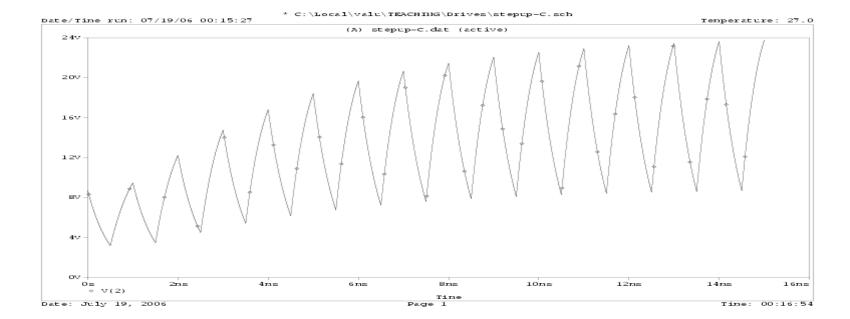


Time

Page 1

Time: 00:15:09

Date: July 19, 2006



Performance of a step up converter with resistive load (C=0).

$$\begin{aligned} & \text{Mode 1 (On)} \\ & i_1(t) = \frac{V_s}{L}t + I_1, \quad 0 \leq t \leq kT \\ & \text{Mode 2 (Off): , and} \\ & I_2 = i_1(kT) = \frac{V_s}{L}kT + I_1 \quad \text{and} \\ & i_2(t) = I_2e^{-(t-kT)R/L} + \frac{V_s - E}{R}(1 - e^{-(t-kT)R/L}), \quad kT \leq t \leq T. \\ & \text{At steady state } i_1(0) = i_2(T), \\ & I_1 = \frac{V_s}{R}\left(\frac{kze^{(k-1)z}}{1 - e^{(k-1)z}}\right) + \frac{V_s - E}{R} \\ & I_2 = \frac{V_s}{R}\left(\frac{kz}{1 - e^{(k-1)z}}\right) + \frac{V_s - E}{R}, \qquad z = T\frac{R}{L}, \\ & \Delta I = \frac{V_s}{L}kT, \quad I_{a,\text{load}} = \frac{I_1 + I_2}{2}(1 - k) \\ & \frac{E}{V_s} \leq 1 \quad \text{for continuous inductor current} \end{aligned}$$