Helical Springs Subjected to Fatigue Loading

The helical springs subjected to fatigue loading are designed by using the *Soderberg line method. The spring materials are usually tested for torsional endurance strength under a repeated stress that varies from zero to a maximum. Since the springs are ordinarily loaded in one direction only (the load in springs is never reversed in nature), therefore a modified Soderberg diagram is used for springs, as shown in Fig.

The endurance limit for reversed loading is shown at point A where the mean shear stress is equal to $\tau e / 2$ and the variable shear stress is also equal to $\tau e / 2$. A line drawn from A to B (the yield point in shear, τy) gives the Soderberg's failure stress line. If a suitable factor of safety (F.S.) is applied to the yield strength (τy), a safe stress line CD may be drawn parallel to the line AB, as shown in Fig. Consider a design point P on the line CD. Now the value of factor of safety may be obtained as discussed below :





From similar triangles PQD and AOB, we have

$$\frac{PQ}{QD} = \frac{OA}{OB} \quad \text{or} \quad \frac{PQ}{O_1D - O_1Q} = \frac{OA}{O_1B - O_1O}$$
$$\frac{\tau_v}{\frac{\tau_v}{F.S.} - \tau_m} = \frac{\tau_e/2}{\tau_v - \frac{\tau_e}{2}} = \frac{\tau_e}{2\tau_v - \tau_e}$$
$$2 \tau_v \cdot \tau_v - \tau_v \cdot \tau_e = \frac{\tau_e \cdot \tau_v}{F.S.} - \tau_m \cdot \tau_e$$

 $\frac{\tau_{\varepsilon} \cdot \tau_{y}}{F.S.} = 2 \tau_{v} \cdot \tau_{y} - \tau_{v} \cdot \tau_{\varepsilon} + \tau_{m} \cdot \tau_{\varepsilon}$

or

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Dividing both sides by $\tau_{o} \cdot \tau_{y}$ and rearranging, we have

Notes : 1. From equation (i), the expression for the factor of safety (F.S.) may be written as

$$F.S. = \frac{\tau_y}{\tau_m - \tau_v + \frac{2\tau_v \cdot \tau_y}{\tau_e}}$$

2. The value of mean shear stress (τ_m) is calculated by using the shear stress factor (K_s) , while the variable shear stress is calculated by using the full value of the Wahl's factor (K). Thus

Mean shear stress,

where
$$K_{s} = \frac{K_{s} \times \frac{8 W_{m} \times D}{\pi d^{3}}}{K_{s}} = 1 + \frac{1}{2C}; \text{ and } W_{m} = \frac{W_{max} + W_{min}}{2}$$

and variable shear stress, $\tau_{v} = K \times \frac{8 W_{v} \times D}{\pi d^{3}}$
where $K = \frac{4C - 1}{4C - 4} + \frac{0.615}{C}; \text{ and } W_{v} = \frac{W_{max} - W_{min}}{2}$

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