## NIPPING IN LEAF SPRING

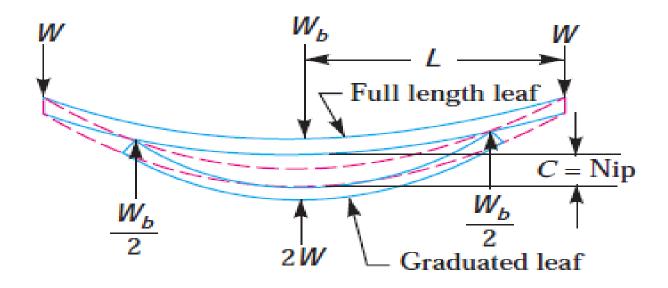
The stress in the full length leaves is 50% greater than the stress in the graduated leaves. In order to utilise the material to the best advantage, all the leaves should be equally stressed.

This condition may be obtained in the following two ways :

**1.** By making the full length leaves of smaller thickness than the graduated leaves. In this way, the full length leaves will induce smaller bending stress due to small distance from the neutral axis to the edge of the leaf.

2. By giving a greater radius of curvature to the full length leaves than graduated leaves, as shown in Fig. before the leaves are assembled to form a spring. By doing so, a gap or clearance will be left between the leaves. This initial gap, as shown by C in Fig. is called **nip. When the central bolt**, holding the various leaves together, is tightened, the full length leaf will bend back as shown dotted in Fig. and have an initial stress in a direction opposite to that of the normal load. The graduated leaves will have an initial stress in the same direction as that of the normal load. When the load is gradually applied to the spring, the full length leaf is first relieved of this initial stress and then stressed in opposite direction. Consequently, the full length leaf will be stressed less than the graduated leaf. The initial gap between the leaves may be adjusted so that under maximum load condition the stress in all the leaves is equal, or if desired, the full length leaves may have the lower stress. This is desirable in automobile springs in which full length leaves are designed for lower stress because the full length leaves carry additional loads caused by the swaying of the car, twisting and in some cases due to driving the car through the rear springs. Let us now find the value of initial gap or nip C.

Consider that under maximum load conditions, the stress in all the leaves is equal. Then at maximum load, the total deflection of the graduated leaves will exceed the deflection of the full length leaves by an amount equal to the initial gap *C. In other words*,



$$\delta_{\rm G} = \delta_{\rm F} + C$$

$$C = \delta_{\rm G} - \delta_{\rm F} = \frac{6 W_{\rm G} \cdot L^3}{n_{\rm G} E \cdot b \cdot t^3} - \frac{4 W_{\rm F} \cdot L^3}{n_{\rm F} \cdot E \cdot b \cdot t^3} \qquad \dots (i)$$
are equal therefore

Since the stresses are equal, therefore

$$\sigma_{\rm G} = \sigma_{\rm F}$$

$$\frac{6 W_{\rm G}.L}{n_{\rm G}.b.t^2} = \frac{6 W_{\rm F}.L}{n_{\rm F}.b.t^2} \quad \text{or} \quad \frac{W_{\rm G}}{n_{\rm G}} = \frac{W_{\rm F}}{n_{\rm F}}$$

$$W_{\rm G} = \frac{n_{\rm G}}{n_{\rm F}} \times W_{\rm F} = \frac{n_{\rm G}}{n} \times W$$

$$n_{\rm E} \qquad n_{\rm F}$$

and

...

...

 $W_{\rm F} = \frac{n_{\rm F}}{n_{\rm G}} \times W_{\rm G} = \frac{n_{\rm F}}{n} \times W$ Substituting the values of  $W_{\rm G}$  and  $W_{\rm F}$  in equation (*i*), we have

The load on the clip bolts  $(W_b)$  required to close the gap is determined by the fact that the gap is equal to the initial deflections of full length and graduated leaves.

$$C = \delta_{\rm F} + \delta_{\rm G}$$

$$\frac{2W.L^3}{n.E.b.t^3} = \frac{4L^3}{n_{\rm F}.E.b.t^3} \times \frac{W_b}{2} + \frac{6L^3}{n_{\rm G}.E.b.t^3} \times \frac{W_b}{2}$$
or
$$\frac{W}{n} = \frac{W_b}{n_{\rm F}} + \frac{3W_b}{2n_{\rm G}} = \frac{2n_{\rm G}.W_b + 3n_{\rm F}.W_b}{2n_{\rm F}.n_{\rm G}} = \frac{W_b (2n_{\rm G} + 3n_{\rm F})}{2n_{\rm F}.n_{\rm G}}$$

$$\therefore \qquad W_b = \frac{2n_{\rm F}.n_{\rm G}.W}{n (2n_{\rm G} + 3n_{\rm F})} \qquad ...(iii)$$

The final stress in spring leaves will be the stress in the full length leaves due to the applied load *minus* the initial stress.

$$\therefore \text{ Final stress,} \qquad \sigma = \frac{6 W_{\text{F}} L}{n_{\text{F}} b t^2} - \frac{6 L}{n_{\text{F}} b t^2} \times \frac{W_b}{2} = \frac{6 L}{n_{\text{F}} b t^2} \left( W_{\text{F}} - \frac{W_b}{2} \right)$$
$$= \frac{6 L}{n_{\text{F}} b t^2} \left[ \frac{3n_{\text{F}}}{2n_{\text{G}} + 3n_{\text{F}}} \times W - \frac{n_{\text{F}} n_{\text{G}} W}{n (2n_{\text{G}} + 3n_{\text{F}})} \right]$$

$$= \frac{6W.L}{bt^2} \left[ \frac{3}{2n_{\rm G} + 3n_{\rm F}} - \frac{n_{\rm G}}{n(2n_{\rm G} + 3n_{\rm F})} \right]$$
$$= \frac{6W.L}{bt^2} \left[ \frac{3n - n_{\rm G}}{n(2n_{\rm G} + 3n_{\rm F})} \right]$$
$$= \frac{6W.L}{bt^2} \left[ \frac{3(n_{\rm F} + n_{\rm G}) - n_{\rm G}}{n(2n_{\rm G} + 3n_{\rm F})} \right] = \frac{6W.L}{n.bt^2} \qquad \dots (iv)$$

... (Substituting  $n = n_{\rm F} + n_{\rm G}$ )