# FLUID MECHANICS FOR MECHANICAL ENGINEERING (ME 208F)

Section C: Flow Through Pipes- III

### **Darcy-Weisbach Equation**

$ au_{ heta}$	ρ	V	μ	D	е
$ML^{-1}T^{-2}$	ML -3	$LT^{1}$	$ML^{-1}T^{-1}$	L	L

$$\tau_0 = F(\rho, V, \mu, D, e)$$
  

$$\pi_4 = F(\pi_1, \pi_2)$$
  
Repeating variables :  $\rho, V, D$   

$$\pi_1 = \text{Re}; \ \pi_2 = \frac{e}{D}; \ \pi_3 = \frac{\tau_0}{\rho V^2}$$
  

$$\frac{\tau_0}{\rho V^2} = F(\text{Re}, \frac{e}{D})$$
  

$$\tau_0 = \rho V^2 F(\text{Re}, \frac{e}{D})$$

$$h_{f} = \frac{4L}{\gamma D} \tau_{0}$$
$$= \frac{4L}{\gamma D} \rho V^{2} F(\text{Re}, \frac{e}{D})$$
$$= \frac{L}{D} \frac{V^{2}}{2g} \left[ 8F(\text{Re}, \frac{e}{D}) \right]$$
$$h_{f} = f \frac{L}{D} \frac{V^{2}}{2g}$$

$$f = 8F(\operatorname{Re}, \frac{e}{D})$$

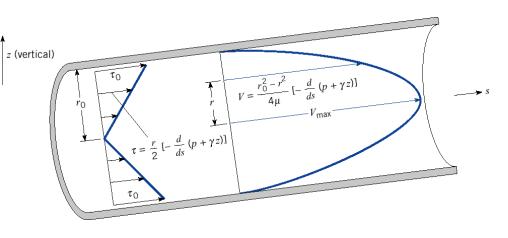
Darcy-Weisbach Eq.

Friction factor

### Laminar Flow in Pipes

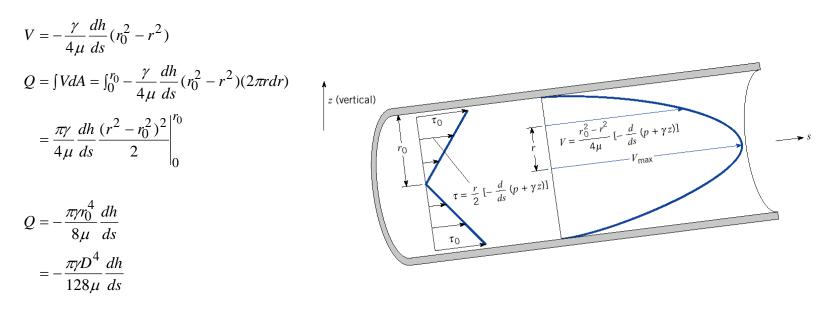
• Laminar flow -- Newton's law of viscosity is valid:

 $\tau = \mu \frac{dV}{dy} = -\frac{r\gamma}{2} \frac{dh}{ds}$   $\frac{dV}{dy} = -\frac{dV}{dr}$   $\frac{dV}{dr} = \frac{r\gamma}{2\mu} \frac{dh}{ds}$   $dV = \frac{r\gamma}{2\mu} \frac{dh}{ds} dr$   $V = \frac{r^2\gamma}{4\mu} \frac{dh}{ds} + C \qquad C = -\frac{r_0^2\gamma}{4\mu} \frac{dh}{ds}$   $V = -\frac{r_0^2\gamma}{4\mu} \frac{dh}{ds} \left[ 1 - \left(\frac{r}{r_0}\right)^2 \right]$   $V = V_{\text{max}} \left[ 1 - \left(\frac{r}{r_0}\right)^2 \right]$ 



 Velocity distribution in a pipe (laminar flow) is parabolic with maximum at center.

### **Discharge in Laminar Flow**



$$\overline{V} = \frac{Q}{A}$$
$$\overline{V} = -\frac{\gamma D^2}{32\mu} \frac{dh}{ds}$$

#### Head Loss in Laminar Flow

$$\overline{V} = -\frac{\gamma D^2}{32\mu} \frac{dh}{ds}$$
$$\frac{dh}{ds} = -\overline{V} \frac{32\mu}{\gamma D^2}$$
$$dh = -\overline{V} \frac{32\mu}{\gamma D^2} ds$$
$$h_2 - h_1 = -\overline{V} \frac{32\mu}{\gamma D^2} (s_2 - s_1)$$
$$h_1 = h_2 + h_f$$

$$h_f = \frac{32\,\mu L\overline{V}}{\gamma D^2}$$

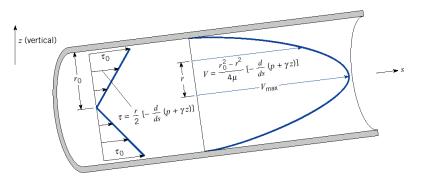
$$h_{f} = \frac{32\mu L\overline{V}}{\gamma D^{2}}$$

$$= \frac{32\mu L\overline{V}}{\gamma D^{2}} \frac{\rho \overline{V}^{2}/2}{\rho \overline{V}^{2}/2}$$

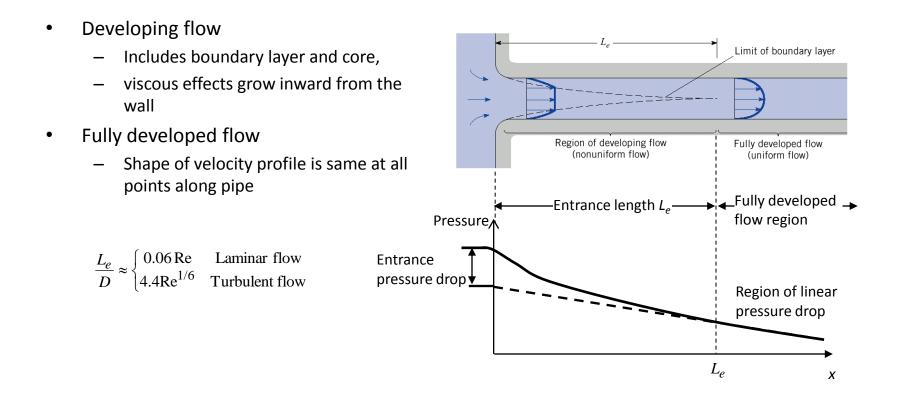
$$= 64(\frac{\mu}{\rho \overline{V} D})(\frac{L}{D})\rho \overline{V}^{2}/2$$

$$= \frac{64}{\text{Re}}(\frac{L}{D})\rho \overline{V}^{2}/2$$

$$h_{f} = f \frac{L}{D} \frac{\rho \overline{V}^{2}}{2} \qquad f = \frac{64}{\text{Re}}$$



### **Pipe Entrance**

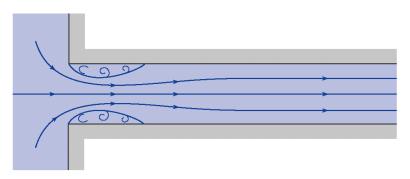


# Entrance Loss in a Pipe

- In addition to frictional losses, there are minor losses due to
  - Entrances or exits
  - Expansions or contractions
  - Bends, elbows, tees, and other fittings
  - Valves
- Losses generally determined by experiment and then corellated with pipe flow characteristics
- Loss coefficients are generally given as the ratio of head loss to velocity head

$$K = \frac{h_L}{\frac{V^2}{2g}}$$
 or  $h_L = K \frac{V^2}{2g}$ 

- K loss coefficent
  - K~0.1 for well-rounded inlet (high Re)
  - K ~ 1.0 abrupt pipe outlet
  - $K \approx 0.5$  abrupt pipe inlet



Abrupt inlet, K ~ 0.5

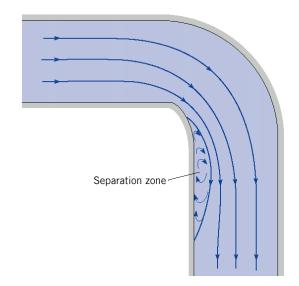
### Elbow Loss in a Pipe

- A piping system may have many minor losses which are all correlated to V<sup>2</sup>/2g
- Sum them up to a total system loss for pipes of the same diameter

$$h_L = h_f + \sum_m h_m = \frac{V^2}{2g} \left[ f \frac{L}{D} + \sum_m K_m \right]$$

• Where,

 $h_L$  = Total head loss  $h_f$  = Frictional head loss  $h_m$  = Minor head loss for fitting m  $K_m$  = Minor head loss coefficient for fitting m



# EGL & HGL for Losses in a Pipe

- Entrances, bends, and other flow transitions cause the EGL to drop an amount equal to the head loss produced by the transition.
- EGL is steeper at entrance than it is downstream of there where the slope is equal the frictional head loss in the pipe.
- The HGL also drops sharply downstream of an entrance

