

Mechanical Failure



Overview

- Failure Modes
 - Fracture, Fatigue, Creep
- Fracture Modes
 - Ductile, Brittle, Intergranular, Transgranular
- Fracture Toughness
- Stress Concentrators (Flaws)
- Crack Propagation

Fracture Modes

- Simple **fracture** is the separation of a body into 2 or more pieces in response to an applied stress that is static (constant) and at temperatures that are low relative to the T_m of the material.
- Classification is based on the ability of a material to experience plastic deformation.
- **Ductile fracture**
 - Accompanied by significant plastic deformation
- **Brittle fracture**
 - Little or no plastic deformation
 - Sudden, catastrophic

Fracture Mechanism

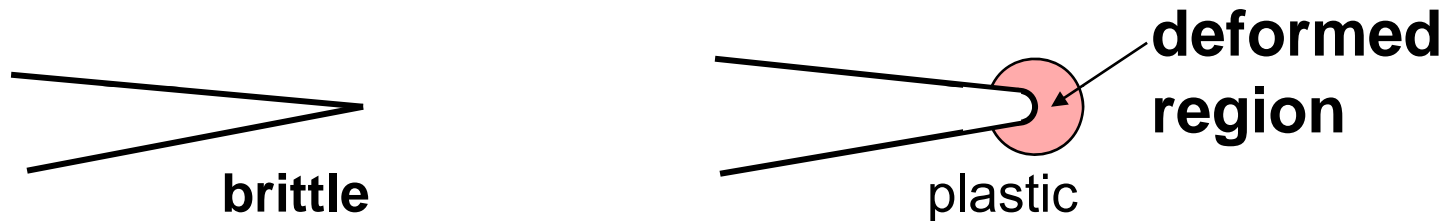
Imposed stress → Crack Formation → Propagation

- **Ductile failure** has extensive plastic deformation in the vicinity of the advancing crack. The process proceeds relatively slow (stable). The crack resists any further extension unless there is an increase in the applied stress.
- In **brittle failure**, cracks may spread very rapidly, with little deformation. These cracks are more unstable and crack propagation will continue without an increase in the applied stress.

Crack Propagation

Cracks propagate due to sharpness of crack tip

- A plastic material deforms at the tip, “blunting” the crack.



Energy balance on the crack

- **Elastic strain energy-**
 - energy stored in material as it is elastically deformed
 - this energy is released when the crack propagates
 - creation of new surfaces requires energy

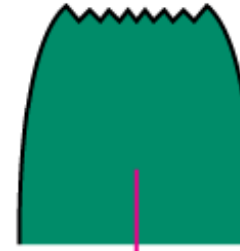
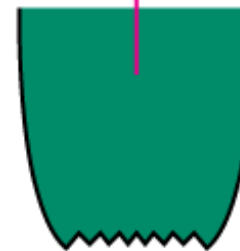
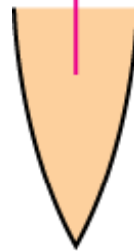
Ductile vs Brittle Failure

Fracture
behavior:

Very
Ductile

Moderately
Ductile

Brittle



$\%AR$ or $\%EL$

Large

Moderate

Small

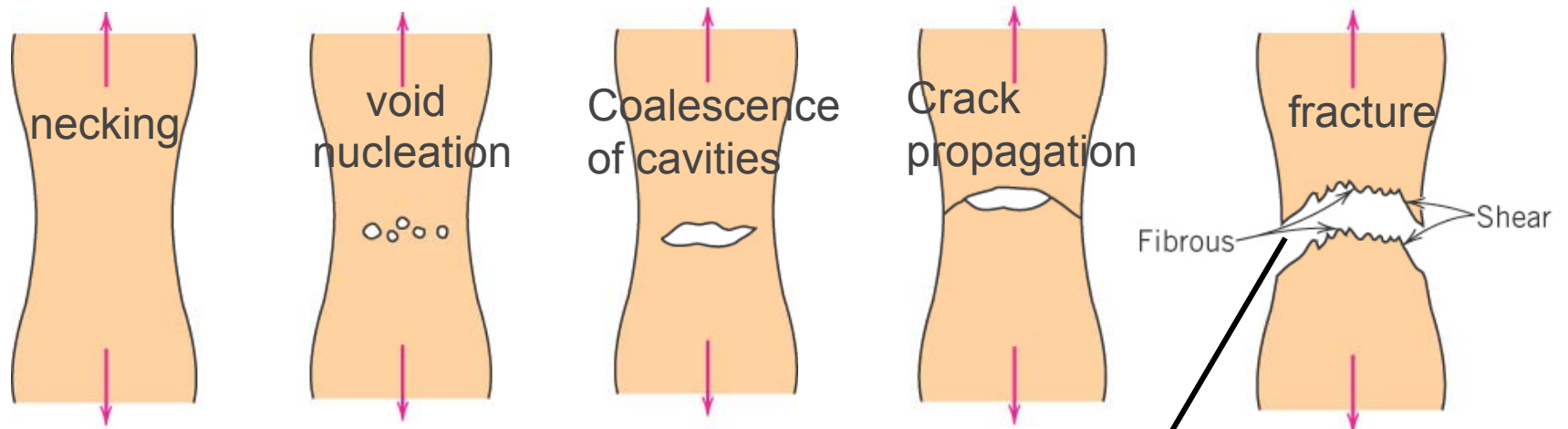
- Ductile fracture is usually more desirable than brittle fracture.

Ductile:
Warning before
fracture

Brittle:
No
warning

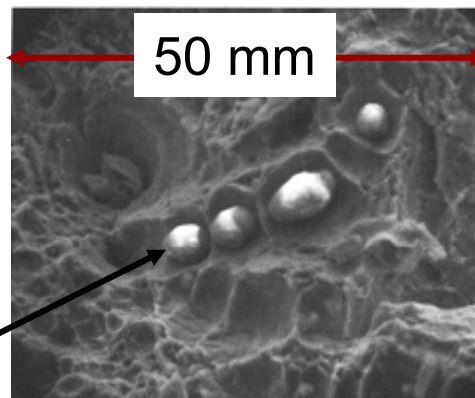
Moderately Ductile Failure

- Evolution to failure:

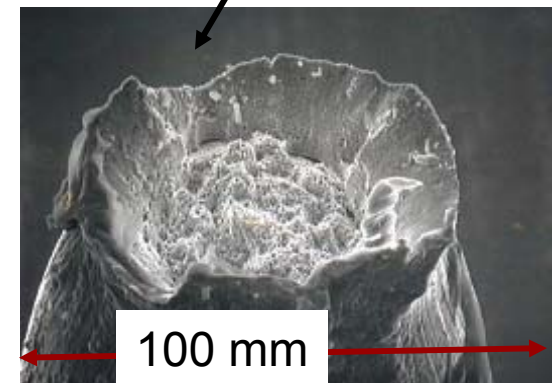


- Resulting fracture surfaces (steel)

particles serve as void nucleation sites.



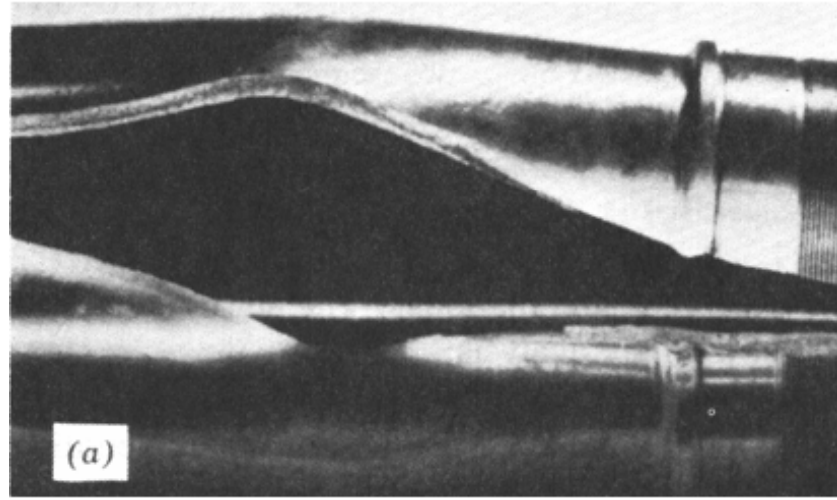
From V.J. Colangelo and F.A. Heiser, *Analysis of Metallurgical Failures* (2nd ed.), Fig. 11.28, p. 294, John Wiley and Sons, Inc., 1987. (Orig. source: P. Thornton, *J. Mater. Sci.*, Vol. 6, 1971, pp. 347-56.)



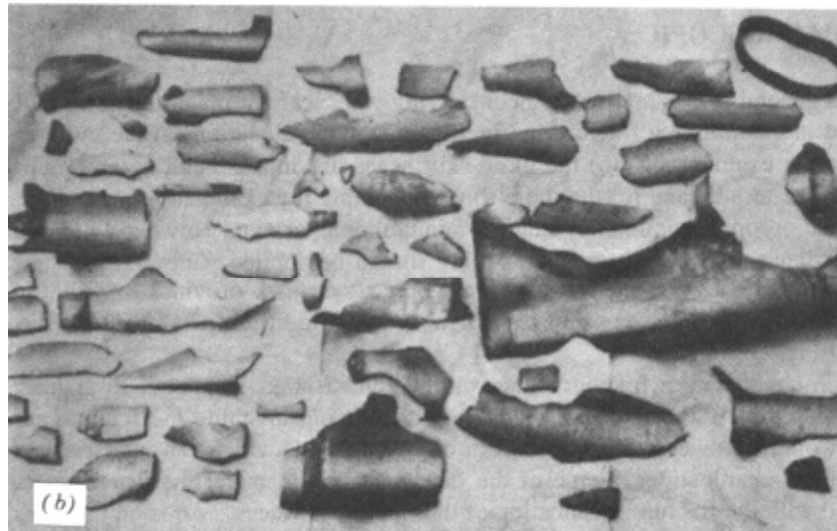
Fracture surface of tire cord wire loaded in tension. Courtesy of F. Roehrig, CC Technologies, Dublin, OH. Used with permission.

Example: Pipe Failures

- **Ductile failure:**
 - one piece
 - large deformation



- **Brittle failure:**
 - many pieces
 - small deformations



Figures from V.J. Colangelo and F.A. Heiser, *Analysis of Metallurgical Failures* (2nd ed.), Fig. 4.1(a) and (b), p. 66 John Wiley and Sons, Inc., 1987. Used with permission.

Ductile vs. Brittle Failure



(a)

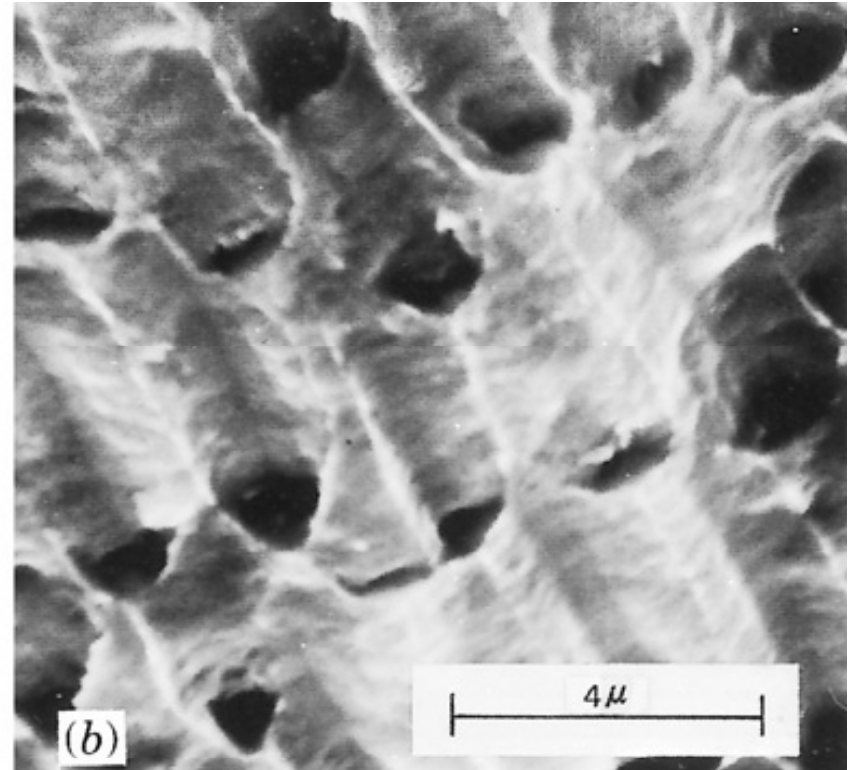
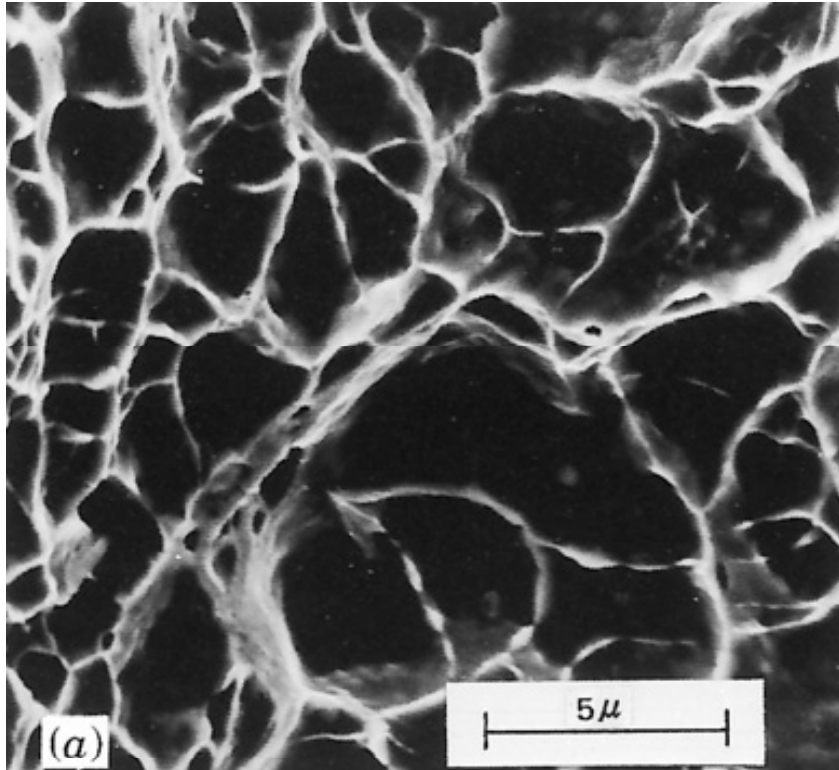
cup-and-cone fracture



(b)

brittle fracture

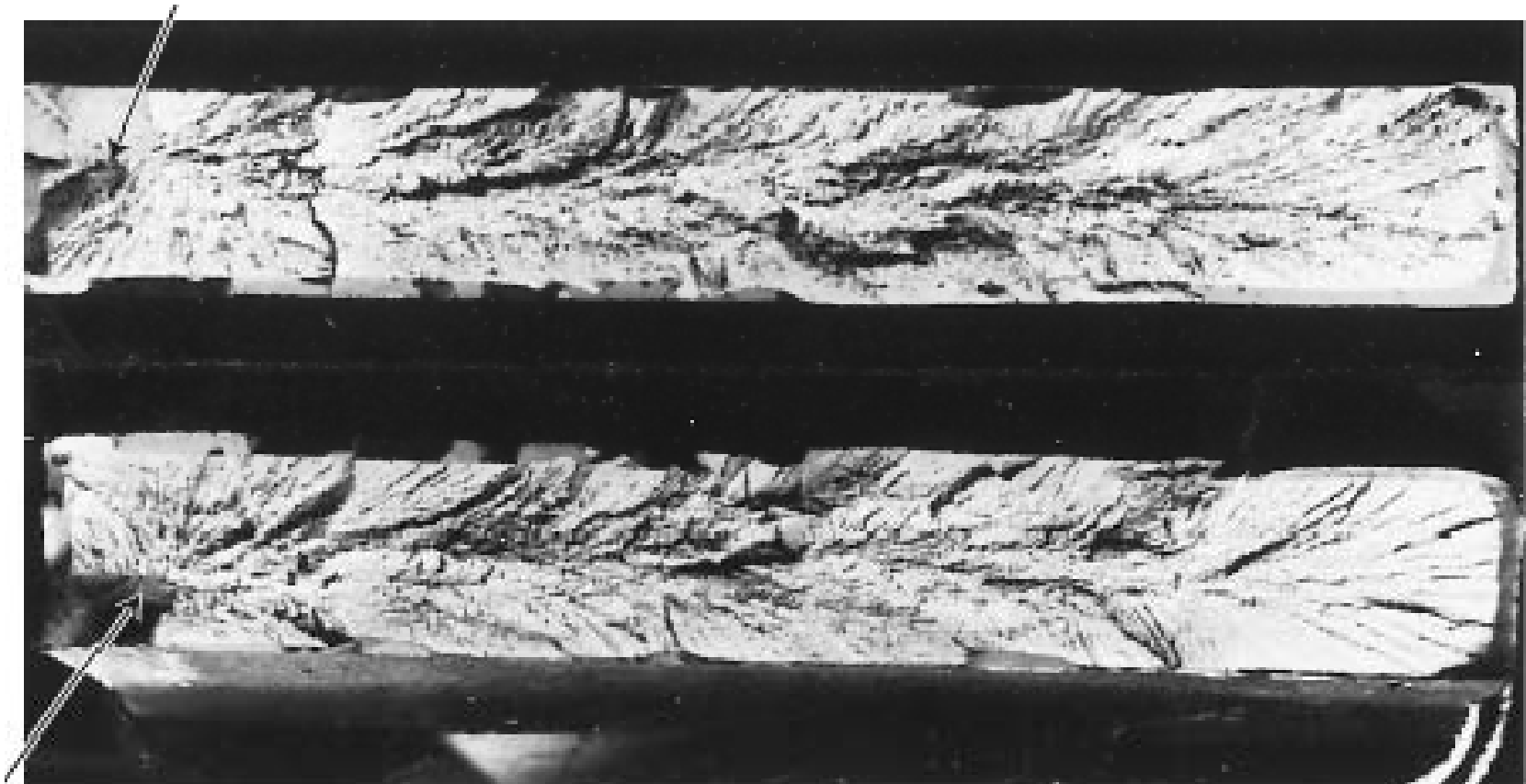
Ductile Failure



(a) SEM image showing spherical dimples resulting from a uniaxial tensile load. (b) SEM image of parabolic dimples from shear loading.

Brittle Fracture

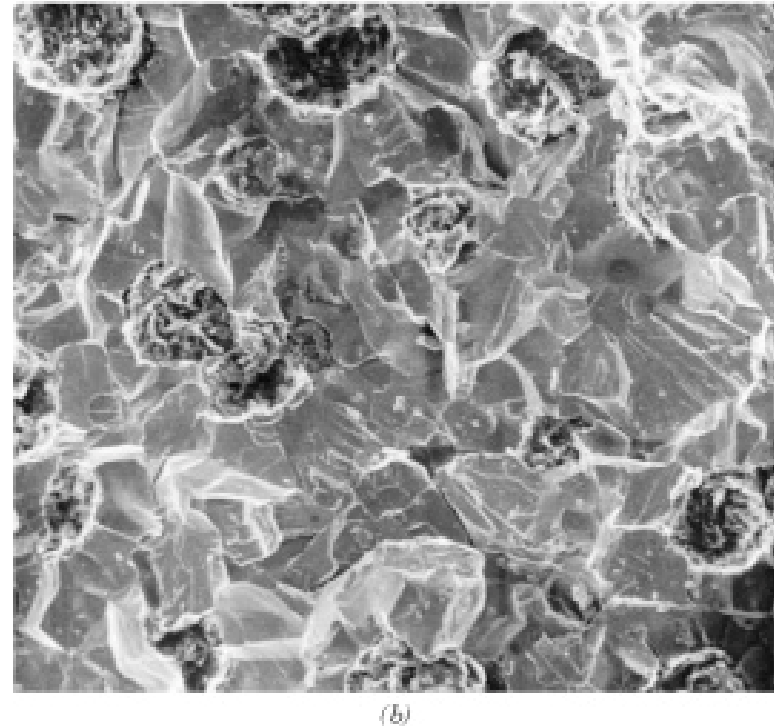
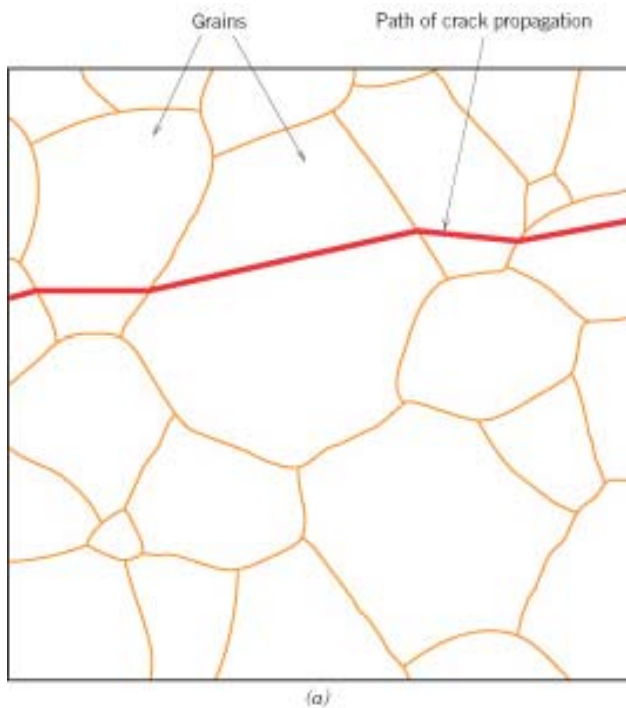
Arrows indicate point at failure origination



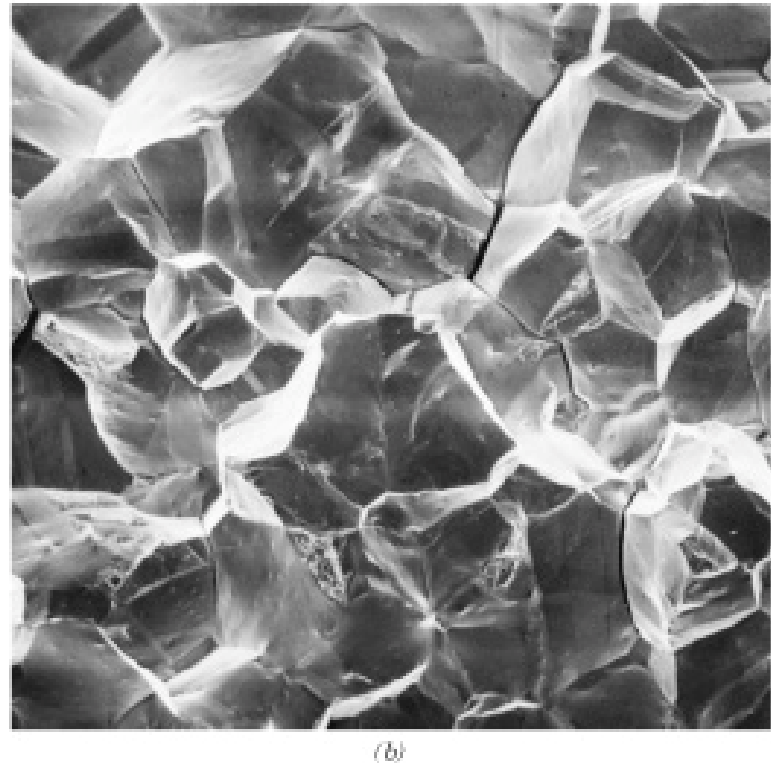
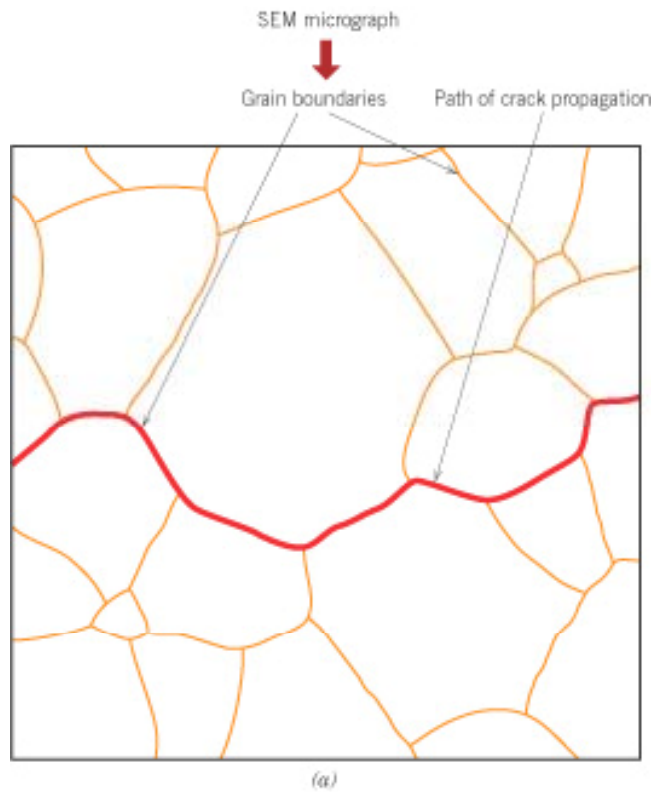
Distinctive pattern on the fracture surface: V-shaped “chevron” markings point to the failure origin.

Transgranular Fracture

- Cleavage - in most brittle crystalline materials, crack propagation that results from the **repeated breaking of atomic bonds** along specific planes.
- This leads to transgranular fracture where the **crack splits (cleaves) through the grains**.



Intergranular Fracture



- Intergranular failure is typically due to elemental depletion (chromium) at the grain boundaries or some type of weakening of the grain boundary due to chemical attack, oxidation, embrittlement.

Fracture Mechanics

Studies the relationships between:

- ❑ material properties
- ❑ stress level
- ❑ crack producing flaws
- ❑ crack propagation mechanisms

Stress Concentration

- The **measured fracture strengths** for most **brittle materials** are significantly lower than those **predicted** by theoretical **calculations** based on atomic bond energies.
- This discrepancy is explained by the presence of very small, **microscopic flaws** or **cracks** that are inherent to the material.
- The flaws act as **stress concentrators** or **stress raisers**, amplifying the stress at a given point.
- This localized stress diminishes with distance away from the crack tip.

Fracture Toughness

- Fracture toughness measures a material's **resistance to brittle fracture** when a crack is present.
- It is an indication of the amount of stress required to propagate a **preexisting flaw**.
- Flaws may appear as **cracks, voids, metallurgical inclusions, weld defects, design discontinuities**, or some combination thereof.
- It is common practice to assume that flaws are present and use the **linear elastic fracture mechanics (LEFM)** approach to **design critical components**.
- This approach uses the flaw size and features, component geometry, loading conditions and the **fracture toughness** to evaluate the ability of a component containing a flaw to resist fracture.

Ductile vs Brittle

- The effect of a stress raiser is more significant in brittle than in ductile materials.
- For a ductile material, plastic deformation results when the maximum stress exceeds the yield strength.
- This leads to a more uniform distribution of stress in the vicinity of the stress raiser; the maximum stress concentration factor will be less than the theoretical value.
- In brittle materials, there is no redistribution or yielding.

Fracture Toughness

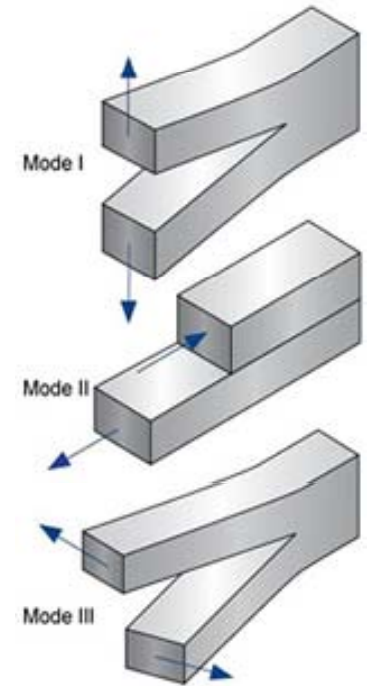
Table 9.1 Room-Temperature Yield Strength and Plane Strain Fracture Toughness Data for Selected Engineering Materials

<i>Material</i>	<i>Yield Strength</i>		<i>K_{Ic}</i>	
	<i>MPa</i>	<i>ksi</i>	<i>MPa√m</i>	<i>ksi√in.</i>
Metals				
Aluminum alloy ^a (7075-T651)	495	72	24	22
Aluminum alloy ^a (2024-T3)	345	50	44	40
Titanium alloy ^a (Ti-6Al-4V)	910	132	55	50
Alloy steel ^a (4340 tempered @ 260°C)	1640	238	50.0	45.8
Alloy steel ^a (4340 tempered @ 425°C)	1420	206	87.4	80.0
Ceramics				
Concrete	—	—	0.2–1.4	0.18–1.27
Soda-lime glass	—	—	0.7–0.8	0.64–0.73
Aluminum oxide	—	—	2.7–5.0	2.5–4.6
Polymers				
Polystyrene (PS)	25.0–69.0	3.63–10.0	0.7–1.1	0.64–1.0
Poly(methyl methacrylate) (PMMA)	53.8–73.1	7.8–10.6	0.7–1.6	0.64–1.5
Polycarbonate (PC)	62.1	9.0	2.2	2.0

^a **Source:** Reprinted with permission, *Advanced Materials and Processes*, ASM International, © 1990.

stress-intensity factor (K)

- The stress-intensity factor (K) is used to determine the fracture toughness of most materials.
- A Roman numeral subscript indicates the mode of fracture and the three modes of fracture are illustrated in the image to the right.
- **Mode I** fracture is the condition where the **crack plane is normal to the direction of largest tensile loading**. This is the most commonly encountered mode.
- The stress intensity factor is a **function of loading, crack size, and structural geometry**. The stress intensity factor may be represented by the following equation:
$$K_I = \sigma \sqrt{\pi a \beta}$$



K_I is the fracture toughness in $MPa\sqrt{m}$ ($psi\sqrt{in}$)

σ is the applied stress in MPa or psi

a is the crack length in meters or inches

β is a crack length and component geometry factor that is different for each specimen, dimensionless.

Critical Stress

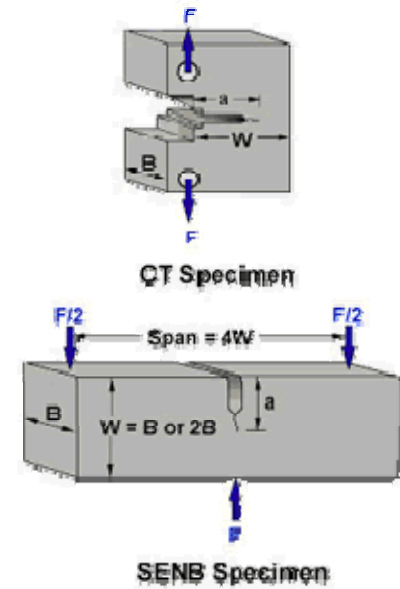
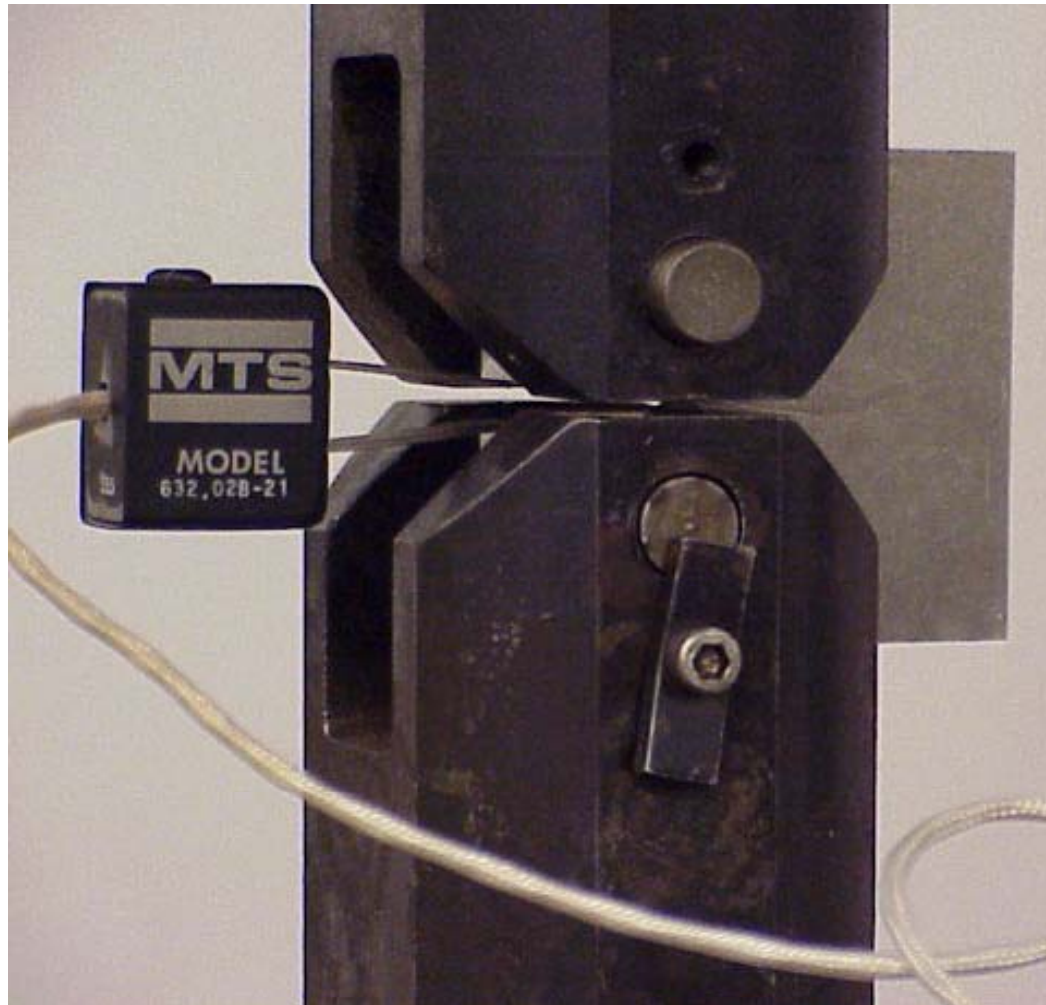
- All brittle materials contain a **population of small cracks and flaws** that have a variety of sizes, geometries and orientations.
- When the magnitude of a tensile stress at the tip of one of these flaws exceeds the value of this critical stress, a crack forms and then propagates, leading to failure.
- Condition for crack propagation:

$$K \geq K_c$$

Stress Intensity Factor:
--Depends on load & geometry.

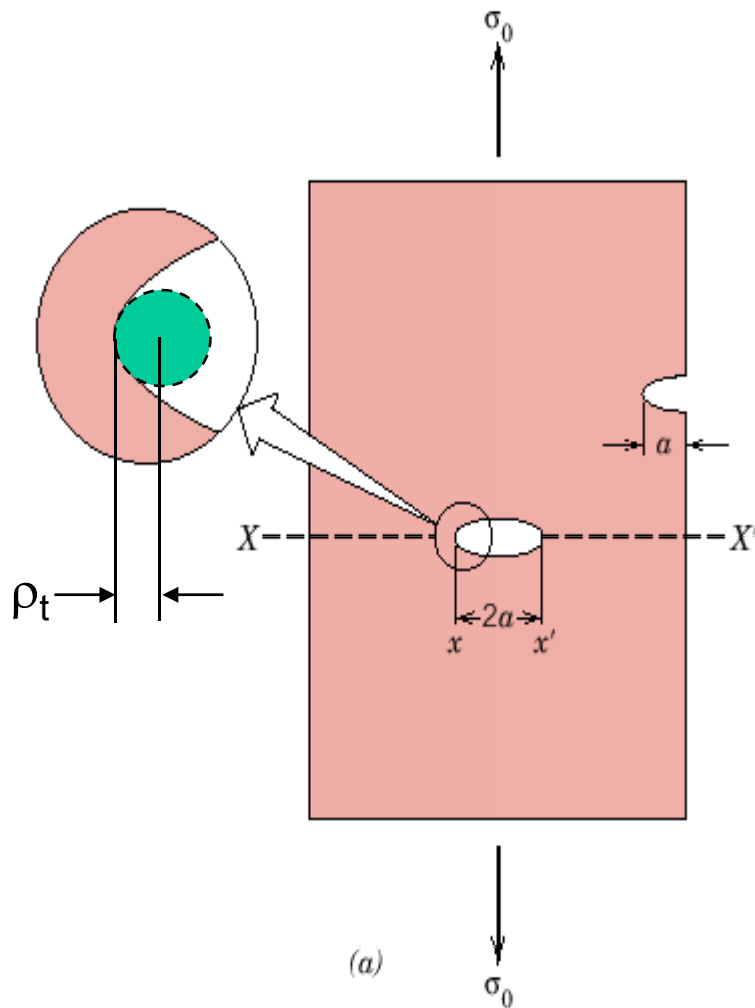
Fracture Toughness:
--Depends on the material, temperature, environment & rate of loading.

Compact tension (CT) specimen



single edge notch
bend (SENB or
three-point bend)

Flaws are Stress Concentrators



If the crack is similar to an elliptical hole through plate, and is oriented perpendicular to applied stress, the **maximum stress** $\sigma_m =$

$$\sigma_m = 2\sigma_o \left(\frac{a}{\rho_t} \right)^{1/2} = K_t \sigma_o$$

where

ρ_t = radius of curvature

σ_o = applied stress

σ_m = stress at crack tip

a = length of surface crack or $\frac{1}{2}$ length of internal crack

$\sigma_m / \sigma_o = K_t$ the stress concentration factor

DESIGN AGAINST CRACK GROWTH

- Crack growth condition: $K \geq K_c$

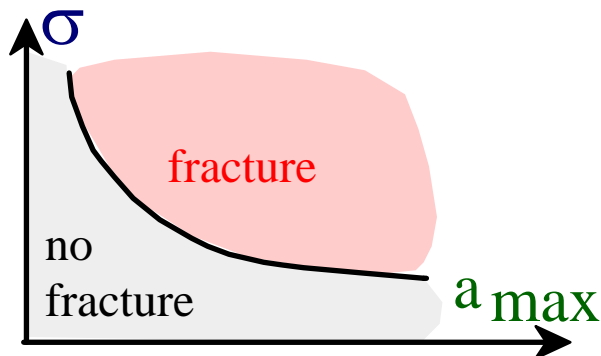
$$Y\sigma\sqrt{\pi a}$$



- Largest, most stressed cracks grow first.

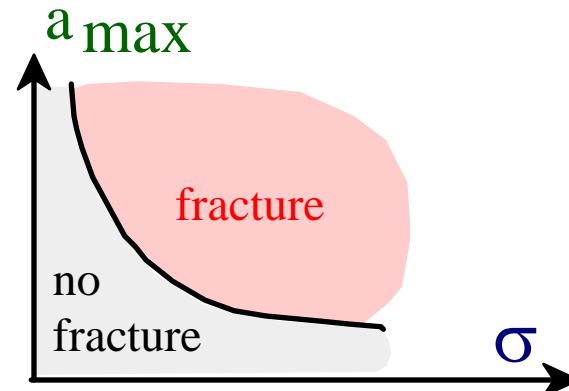
--Result 1: Max flaw size dictates design stress.

$$\sigma_{\text{design}} < \frac{K_c}{Y\sqrt{\pi a_{\text{max}}}}$$



--Result 2: Design stress dictates max. flaw size.

$$a_{\text{max}} < \frac{1}{\pi} \left(\frac{K_c}{Y\sigma_{\text{design}}} \right)^2$$



Design Example: Aircraft Wing

- Material has $K_c = 26 \text{ MPa}\cdot\text{m}^{0.5}$
- Two designs to consider...

Design A

- largest flaw is 9 mm
- failure stress = 112 MPa

Design B

- use same material
- largest flaw is 4 mm
- failure stress = ?

- Use...

$$\sigma_c = \frac{K_c}{Y \sqrt{\pi a_{max}}}$$

- Key point: Y and K_c are the same in both designs. Y is a dimensionless parameter; see Callister page 298.

-- Result:

$$\left(\overset{112 \text{ MPa}}{\sigma_c} \sqrt{\overset{9 \text{ mm}}{a_{max}}} \right)_A = \left(\sigma_c \sqrt{\overset{4 \text{ mm}}{a_{max}}} \right)_B$$

Answer: $(\sigma_c)_B = 168 \text{ MPa}$

- Reducing flaw size pays off.

Sensors made to mesh with plane

- Structural engineers have long imagined the day when materials used in an aircraft, a wind turbine blade or a bridge could sense if they had been strained to the point of damage, reducing their load-carrying capacity, and report that information in real time before the structure's safety is compromised.
- For many years, such a scenario was more the stuff of science fiction than fact, but today, structural health monitoring (SHM) systems that can perform these tasks are closer to reality.
- Scientists have created a fiber mesh embedded with sensors designed to monitor an airplane's structural integrity and outside temperature.
- When wrapped around an aircraft, the sensors could help prevent microscopic cracks from developing into catastrophic failures.
- Made from a plastic polymer, the mesh is designed so it doesn't add significant weight or drag to an aircraft.
- The technology also could be used in autos, packaging and medical devices.

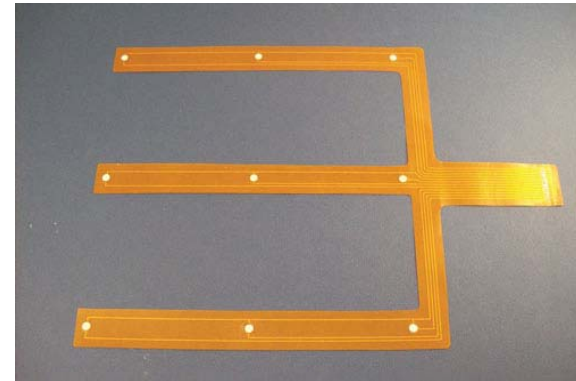
Structural health monitoring (SHM) systems can be arrayed in similar fashion to the human nervous system, with sensors concentrated in key areas where loads are highest.



A comparative vacuum-monitoring (CVM) sensor, is a thin, self-adhesive rubber patch that detects cracks in the underlying material. The rubber is laser-etched with rows of tiny, interconnected channels or galleries, to which an air pressure is applied. Any propagating crack under the sensor breaches the galleries and the resulting change in pressure is monitored.



A piezoelectric-based sensor system from Acellent Technologies, called SMART Layer, identifies damage with small ceramic actuators



An FAA-sponsored study on curved honeycomb-cored panels showed that acoustic emission (AE) monitoring is a reliable method for locating damage initiation sites and for tracking crack progression. Source: Physical Acoustics Corp

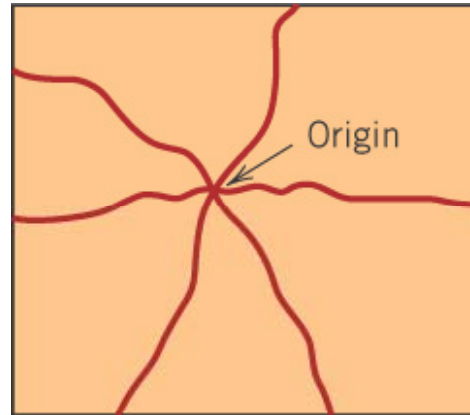


Table 9.2 A List of Several Common Nondestructive Testing (NDT) Techniques

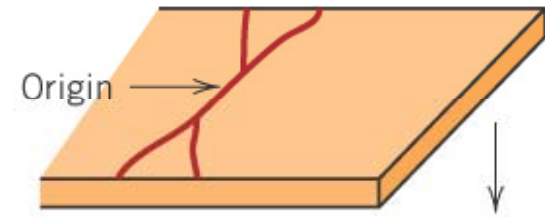
<i>Technique</i>	<i>Defect Location</i>	<i>Defect Size Sensitivity (mm)</i>	<i>Testing Location</i>
Scanning electron microscopy (SEM)	Surface	>0.001	Laboratory
Dye penetrant	Surface	0.025–0.25	Laboratory/in-field
Ultrasonics	Subsurface	>0.050	Laboratory/in-field
Optical microscopy	Surface	0.1–0.5	Laboratory
Visual inspection	Surface	>0.1	Laboratory/in-field
Acoustic emission	Surface/subsurface	>0.1	Laboratory/in-field
Radiography (X-ray/ gamma ray)	Subsurface	>2% of specimen thickness	Laboratory/in-field

Brittle Fracture of Ceramics

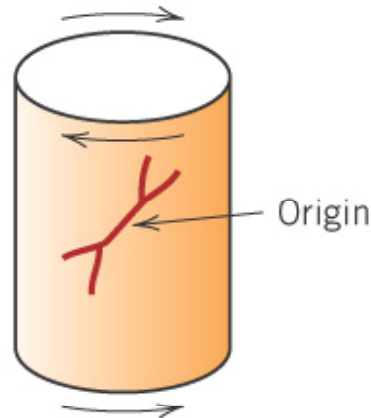
- Most ceramics (at room temperature) fracture before any plastic deformation can occur.
- Typical crack configurations for 4 common loading methods.



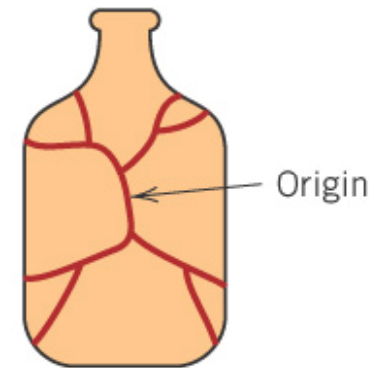
Impact or point loading
(a)



Bending
(b)



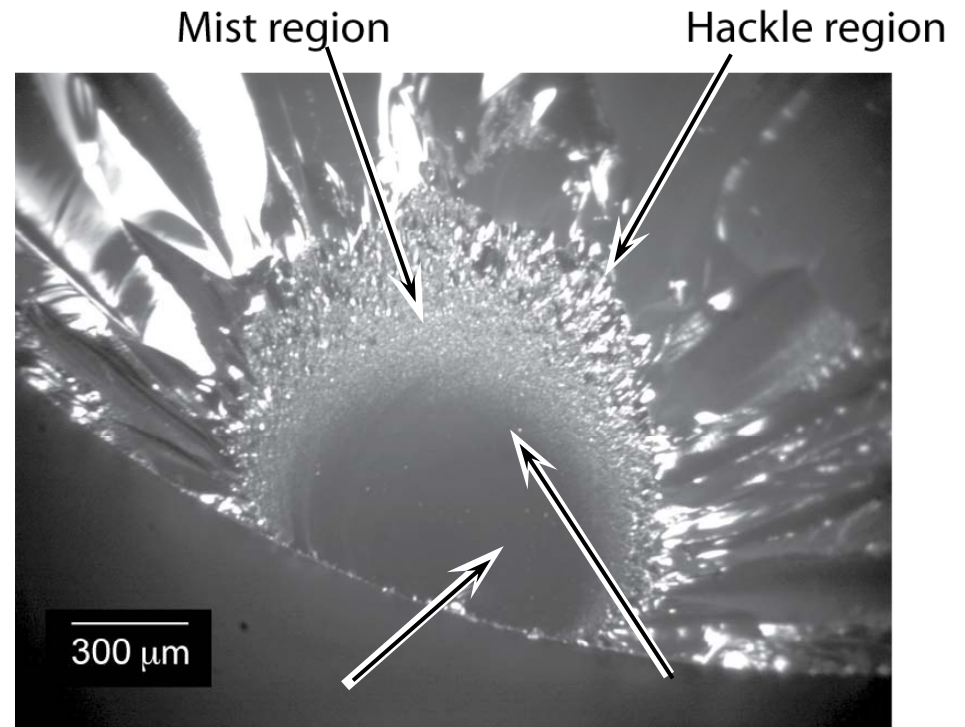
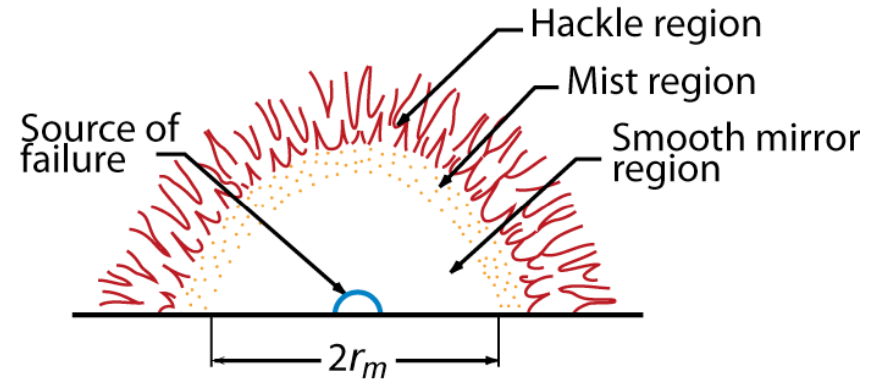
Torsion
(c)



Internal pressure
(d)

Brittle Fracture of Ceramics

- Surface of a 6-mm diameter fused silica rod.
- Characteristic fracture behavior in ceramics
 - Origin point
 - Initial region (**mirror**) is flat and smooth
 - After reaches critical velocity crack branches
 - **mist**
 - **hackle**

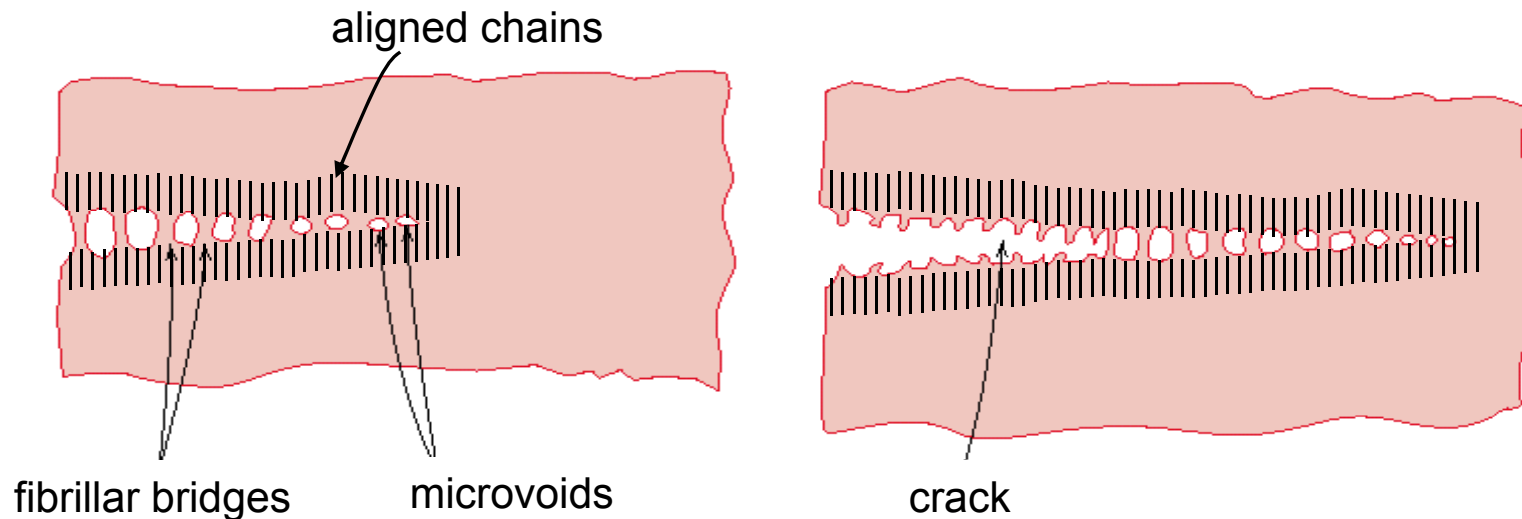


Origin

Mirror region

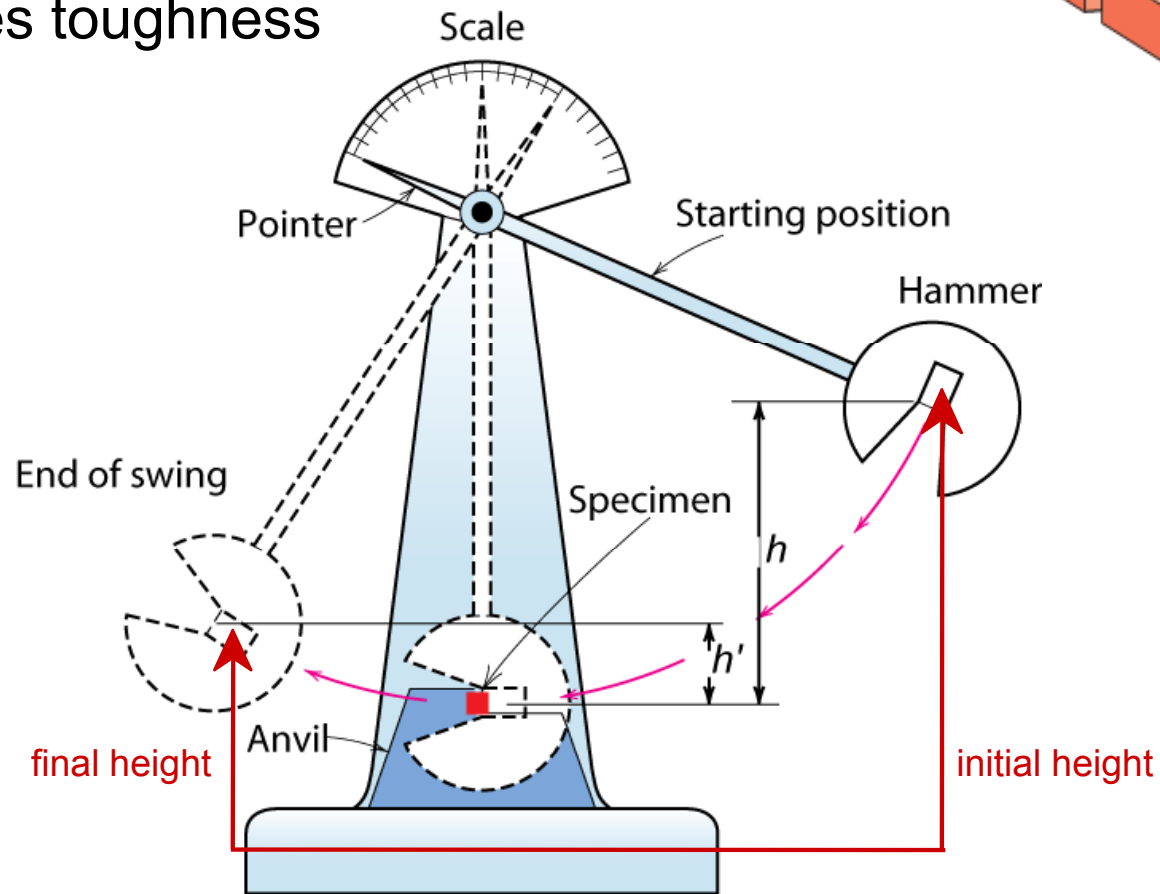
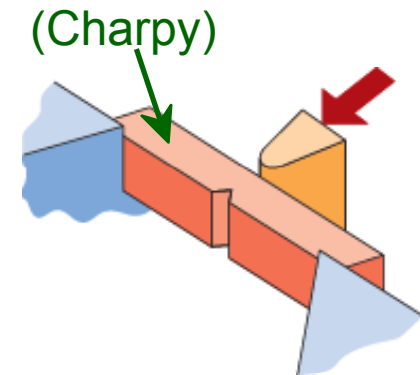
Fracture of Polymers

- ❑ The fracture strengths of polymers are low relative to ceramics and metals.
- ❑ The fracture mode in **thermosetting** polymers (heavily crosslinked networks) is typically brittle.
- ❑ For **thermoplastic** polymers, both ductile and brittle modes are possible. Reduced temperature, increased strain rate, sharp notches, increased specimen thickness are some factors that can influence a brittle fracture.
- ❑ One phenomenon that occurs in thermoplastics is **crazing**, very localized plastic deformation and formation of microvoids and fibrillar bridges



Impact Testing

- Impact loading:
 - severe testing case
 - makes material more brittle
 - decreases toughness

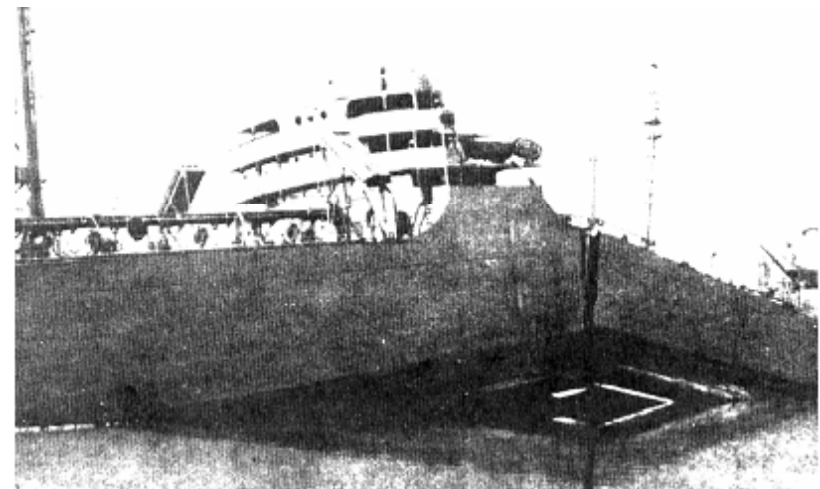


Ductile to Brittle Transition Temperature (DBTT)

- **Pre-WWII: The Titanic**

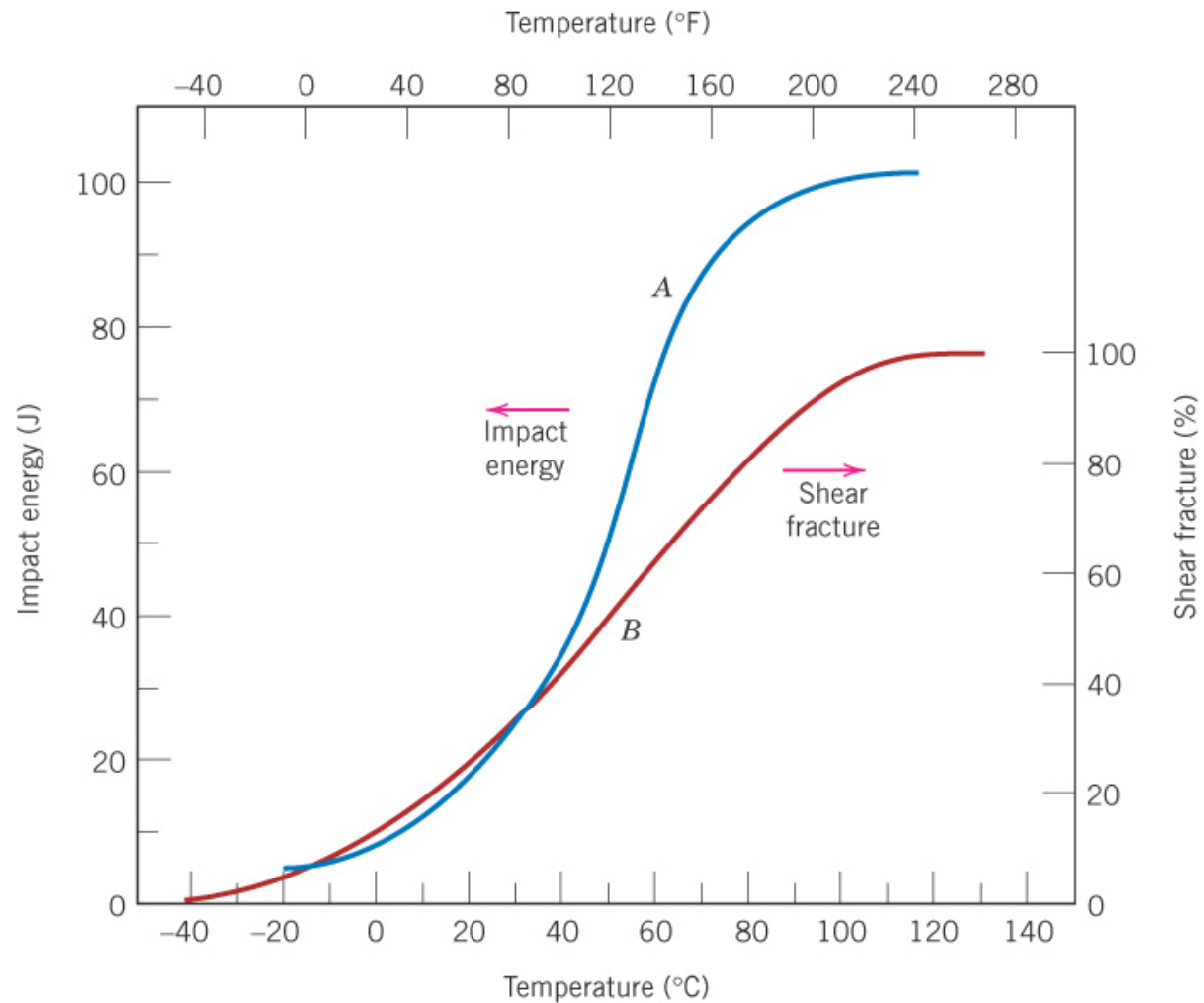


- **WWII: Liberty ships**

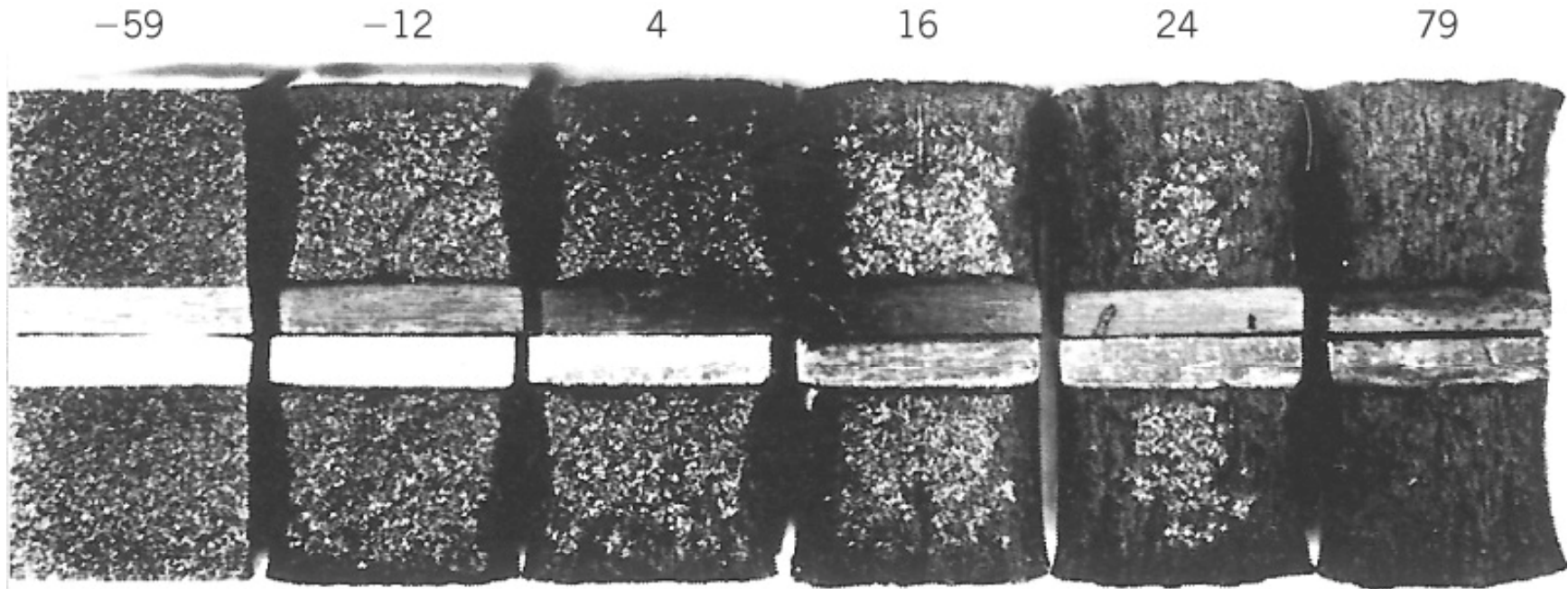


Disastrous consequences for a welded transport ship, suddenly split across the entire girth of the ship (40°F). The vessels were constructed from steel alloys that exhibit a DBTT \approx room temp

Charpy Impact Energy (A) and Shear Fracture % (B) Correlated with Temperature



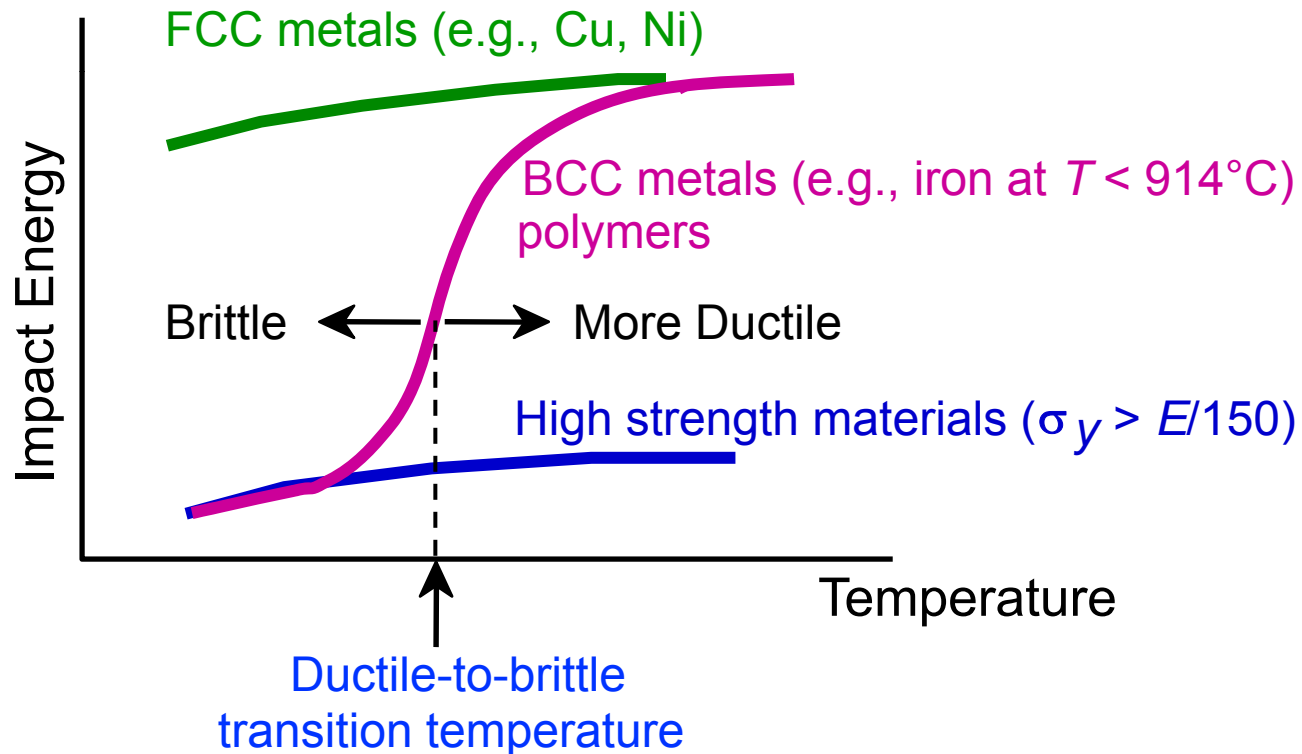
Steel Charpy Samples



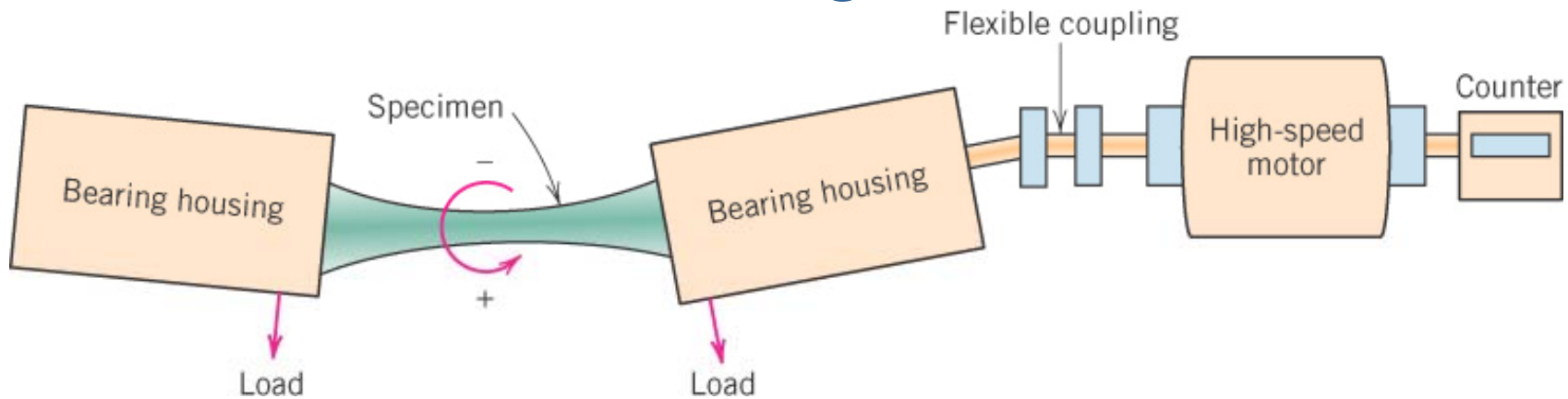
Fracture surfaces after impact showing the variation in ductility with testing temperature ($^{\circ}\text{C}$).

Temperature

- **Increasing temperature...**
 - increases % EL and K_C
- **Ductile-to-Brittle Transition Temperature (DBTT)...**



Fatigue

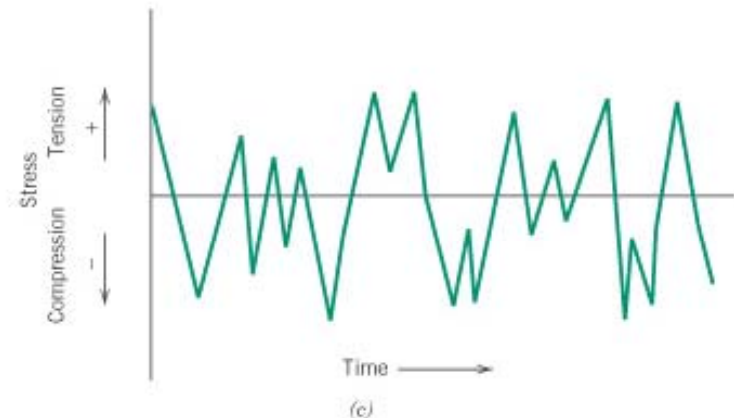
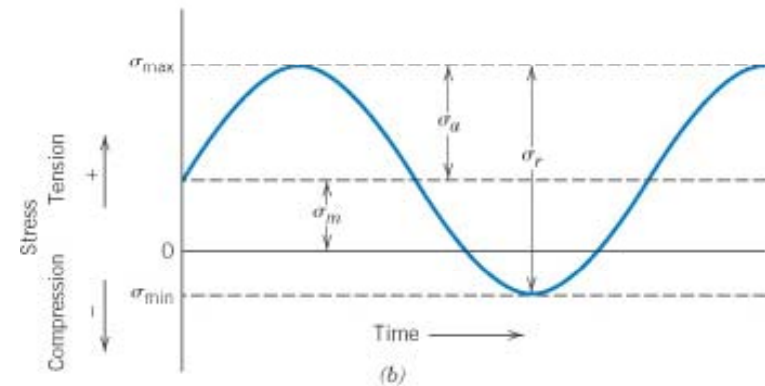
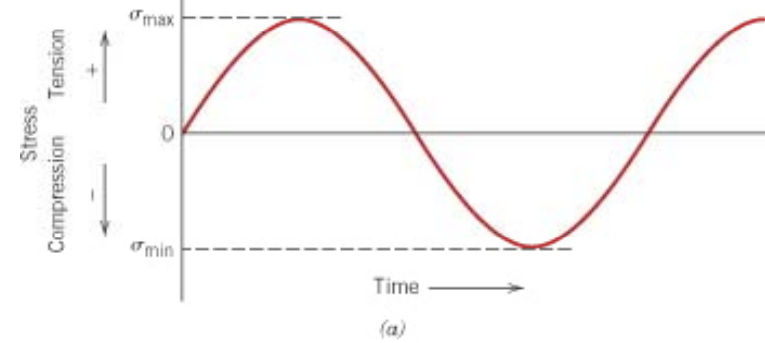


Fatigue testing apparatus for rotating bending test

- ❑ Fatigue is a form of failure that occurs in structures subjected to **dynamic** stresses over an extended period.
- ❑ Under these conditions it is possible to fail at stress levels considerably lower than tensile or yield strength for a static load.
- ❑ Single largest cause of failure in metals; also affects polymers and ceramics.
- ❑ Common failure in bridges, aircraft and machine components.

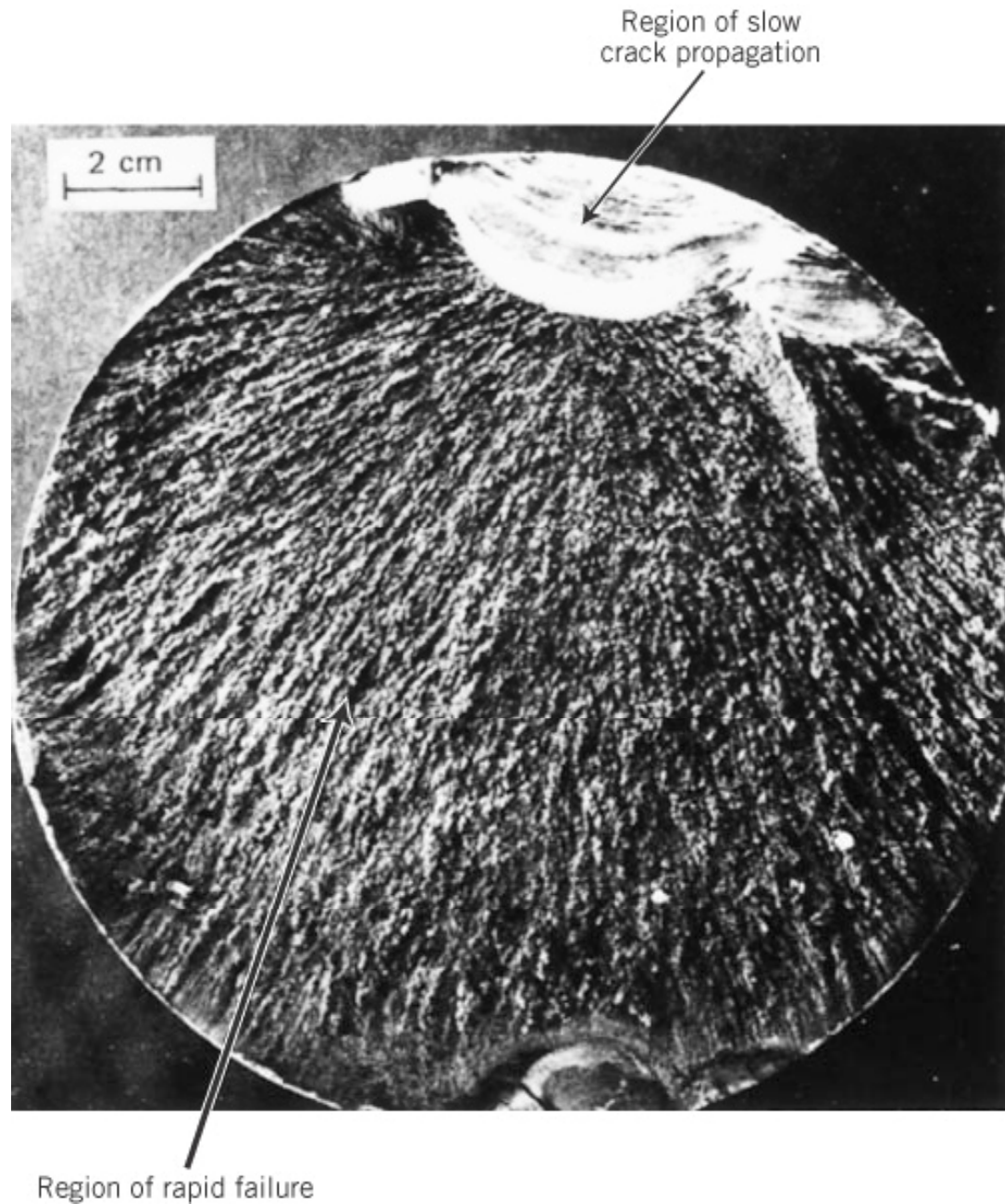
Cyclic Stress - Fatigue

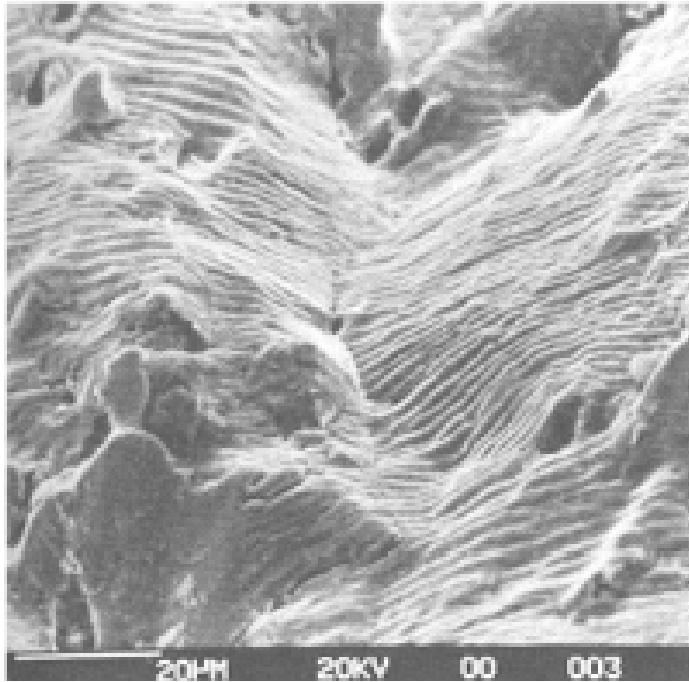
- Variation of stress with time that accounts for fatigue failures.
- The stress may be axial (tension-compression), flexural (bending) or torsional (twisting) in nature.
- There are 3 fluctuating stress-time modes seen in the figure:
(a) reversed stress cycle - **symmetrical** amplitude about a mean zero stress level; (b) repeated stress cycle - **asymmetrical** maxima and minima relative to the zero stress level; (c) variable (**random**) stress level



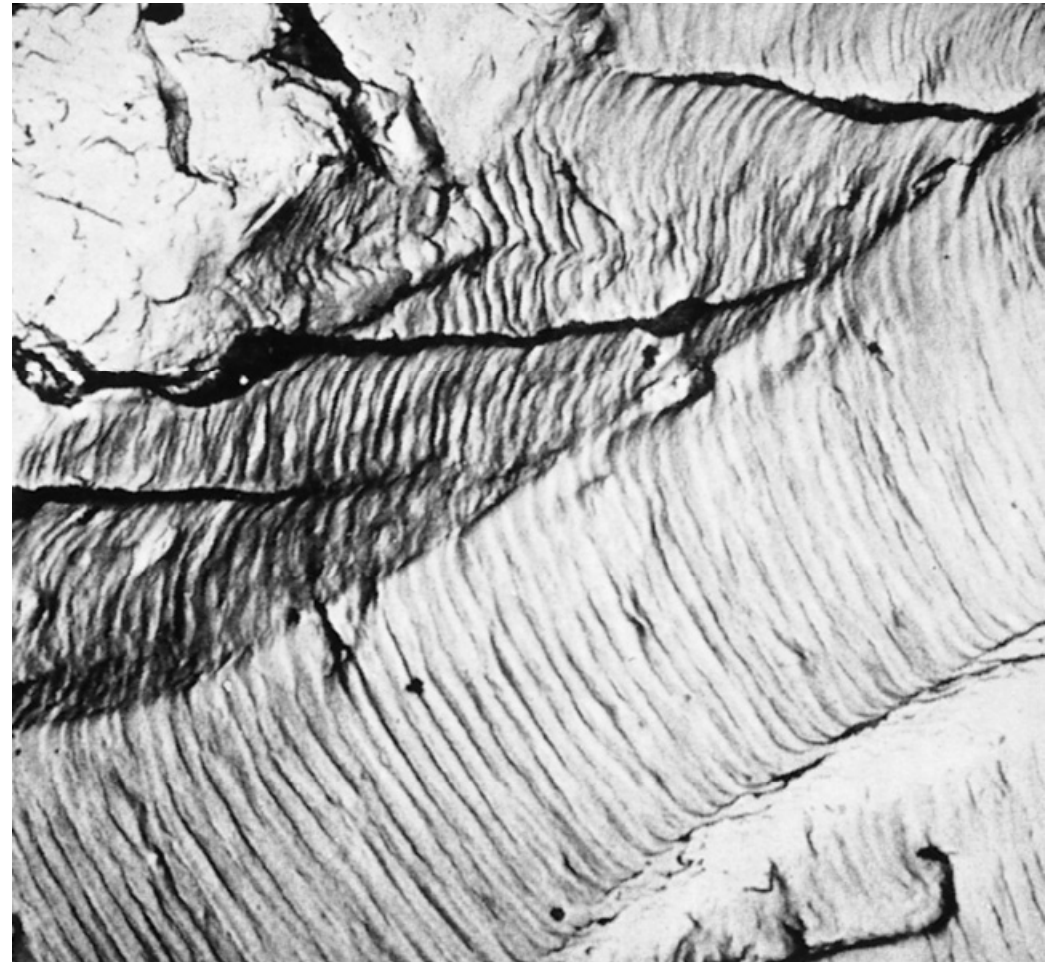
Fatigue

- Fracture surface with crack initiation at top. Surface shows predominantly dull fibrous texture where rapid failure occurred after crack achieved critical size.
- Fatigue failure
 1. Crack initiation
 2. Crack propagation
 3. Final failure

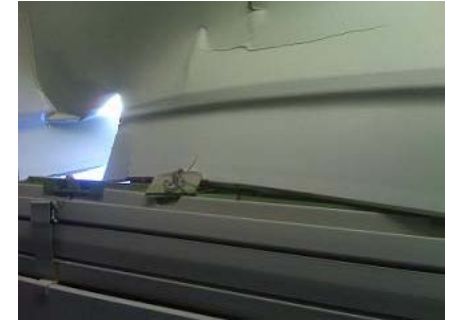




- Striations are close together indicating low stress, many cycles.
- Widely spaced striations mean high stress few cycles.



- Fatigue failure is brittle in nature, even in normally ductile materials; there is very little plastic deformation associated with the failure.
- The image shows fatigue striations (microscopic).



- Federal investigators say **metal fatigue caused a hole to rip open in the roof of a Southwest Airlines jet as it cruised at 35,000 feet last year (2009). The National Transportation Safety Board says the 14-inch crack developed in a spot where two sheets of aluminum skin were bonded together on the Boeing 737 jet.**
- The pilot made an emergency landing in Charleston, W.Va. There were no injuries among the 126 passengers and five crew members. Two months after the scare, Boeing told all airlines with 737s to conduct repeated inspections of the **top of the fuselage near the vertical tail fin.** The Federal Aviation Administration has since made those inspections mandatory.
- Southwest got the plane in 1994 — it's much older than the average Southwest jet — and had **flown it for 50,500 hours and made 42,500 takeoffs and landings** before it sprang a hole in the roof, according to the safety board report. The safety board said it **found signs of metal fatigue by magnifying the area in front of the tail fin. In a 3-inch stretch, the crack penetrated completely through the aluminum skin.**
- FAA records showed that **eight cracks had been found and repaired** in the fuselage during the plane's 14-year checkup.

Fatigue Mechanism

- Crack grows *incrementally*

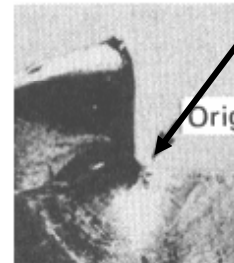
$$\frac{da}{dN} = (\Delta K)^m$$

typ. 1 to 6

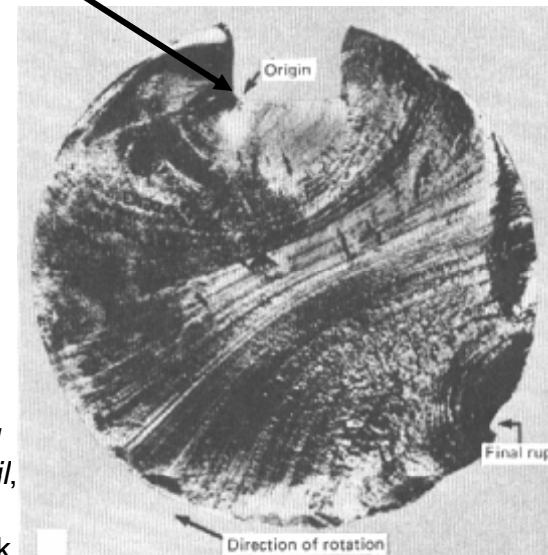
$$\sim (\Delta\sigma)\sqrt{a}$$

increase in crack length per loading cycle

- Failed rotating shaft
 - crack grew even though $K_{max} < K_C$
 - crack grows faster as
 - $\Delta\sigma$ increases
 - crack gets longer
 - loading freq. increases.

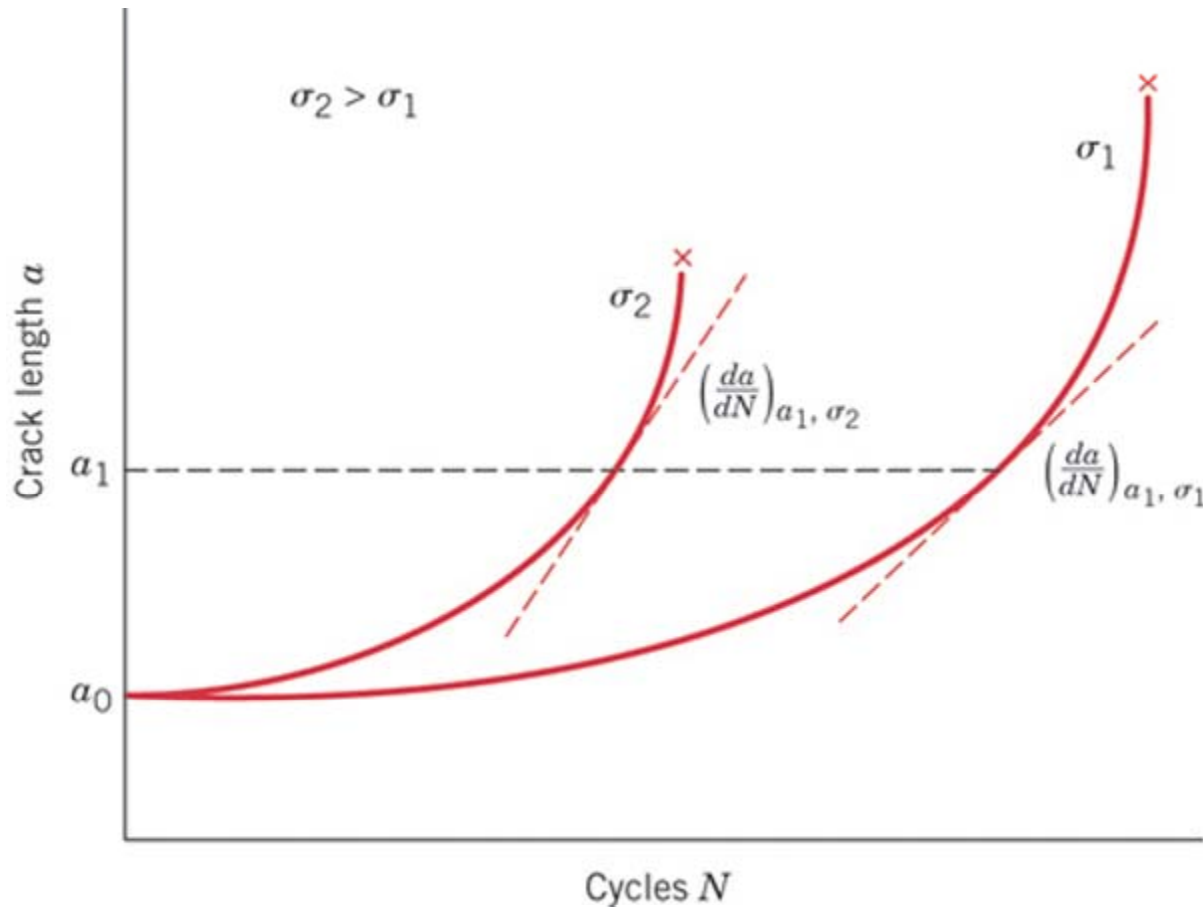


crack origin



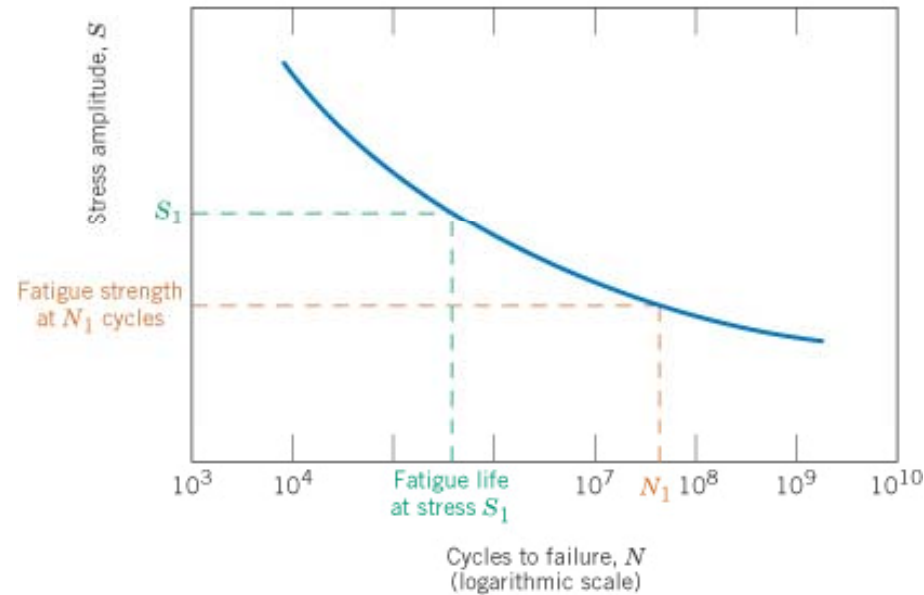
Adapted from Fig. 9.28, Callister & Rethwisch 3e. (Fig. 9.28 is from D.J. Wulpi, *Understanding How Components Fail*, American Society for Metals, Materials Park, OH, 1985.)

Crack growth rate



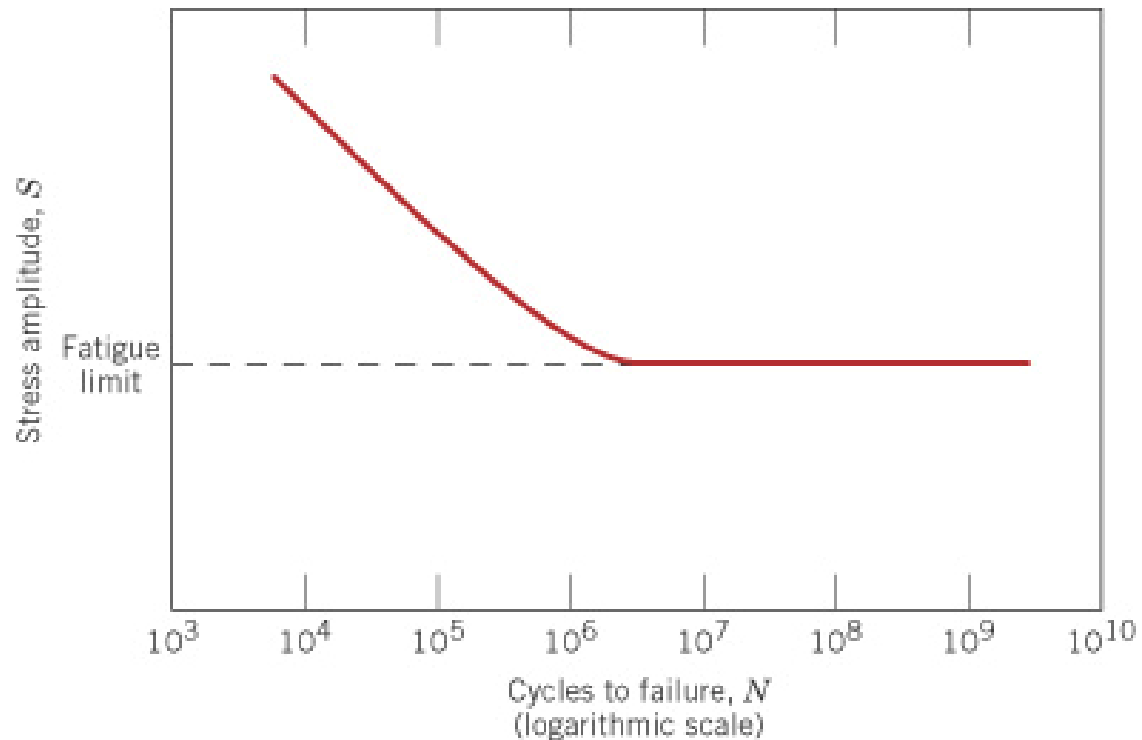
1. Initially, growth rate is small, but increases with increasing crack length.
2. Growth rate increases with applied stress level for a given crack length (a_1).

S-N Curves



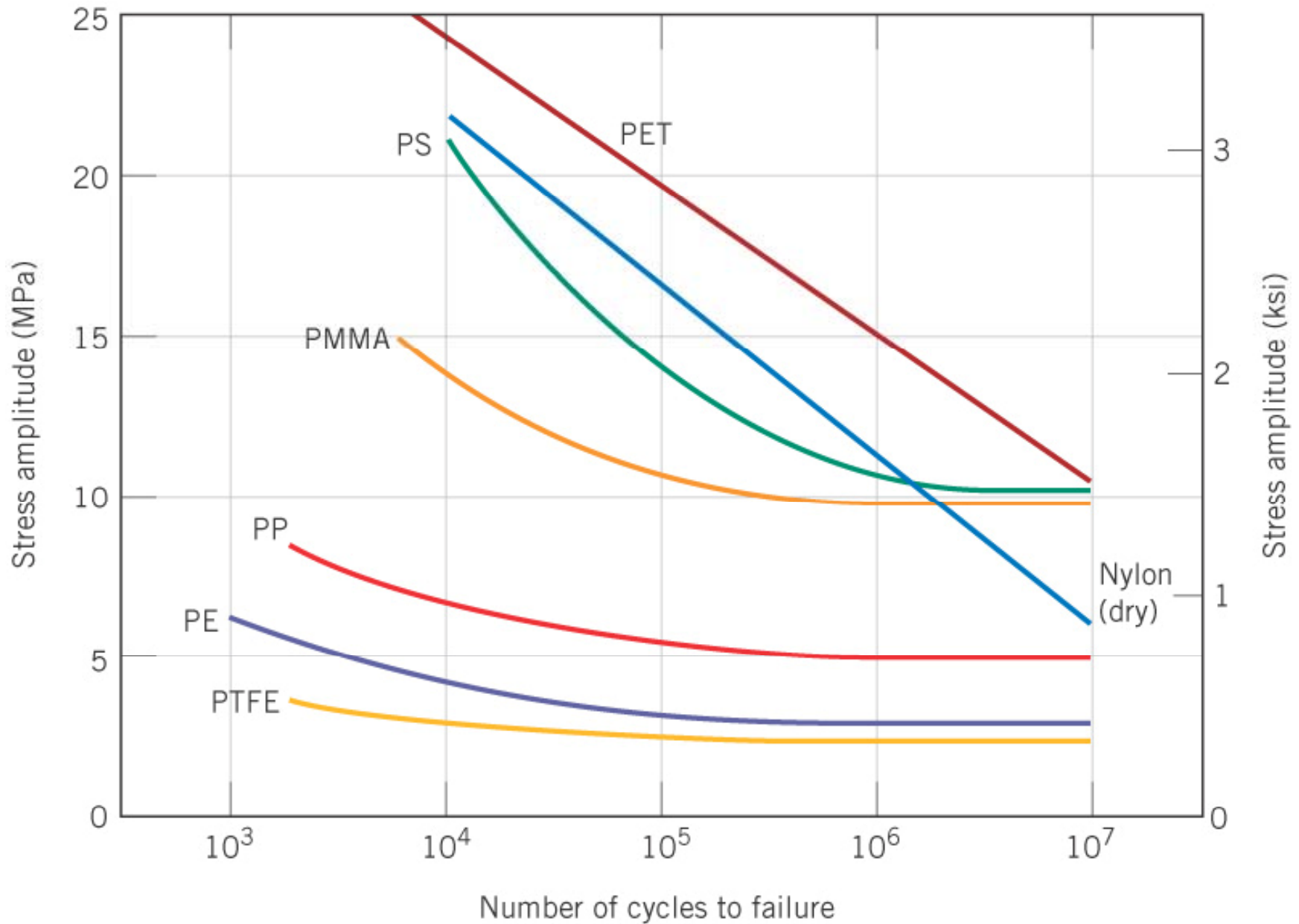
- A specimen is subjected to stress cycling at a maximum stress amplitude; the number of cycles to failure is determined.
- This procedure is repeated on other specimens at progressively decreasing stress amplitudes.
- Data are plotted as stress S versus number N of cycles to failure for all the specimen.
- Typical S-N behavior: the higher the stress level, the fewer the number of cycles.

Fatigue Limit



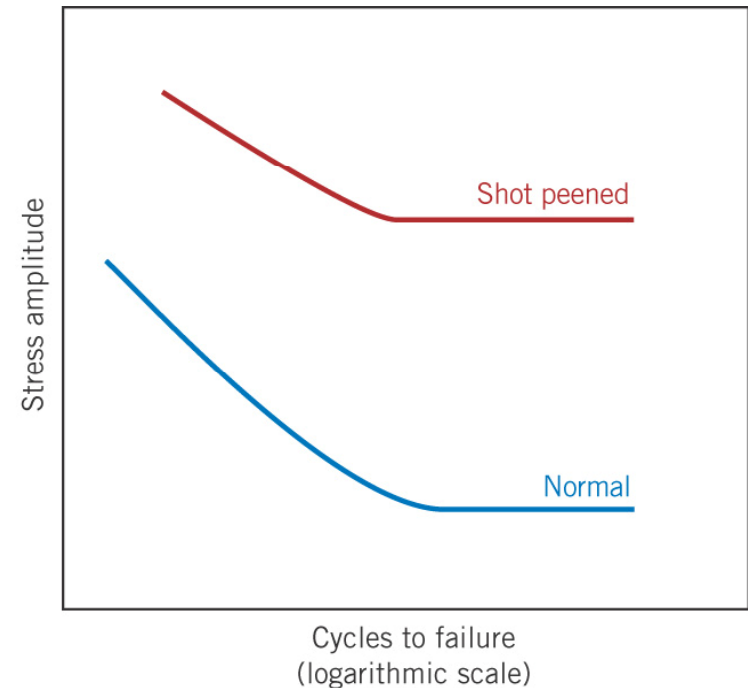
- For some iron and titanium alloys, the S-N curve becomes horizontal at higher number of cycles N .
- Essentially it has reached a fatigue limit, and below this stress level the material will not fatigue.
- The fatigue limit represents the largest value of fluctuating stress that will not cause failure for an infinite number of cycles.

Fatigue Curves for Polymers



Surface Treatments

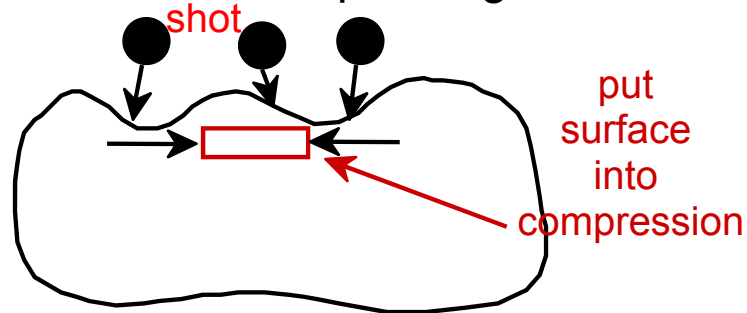
- During machining operations, small scratches and grooves can be introduced; these can limit the fatigue life.
- Improving the surface finish by polishing will enhance fatigue life significantly.
- One of the most effective methods of increasing fatigue performance is by imposing residual compressive stresses within a thin outer surface layer. A surface tensile stress will be offset by the compressive stress.
- **Shot peening** (localized plastic deformation) with small (diameters ranging from 0.1 to 1.0 mm), hard particles (shot) are projected at high velocities on to the surface. The resulting deformation induces compressive stresses to a depth of roughly $\frac{1}{4}$ to $\frac{1}{2}$ of the shot diameter.
- The influence of shot peening is compared in the graph.



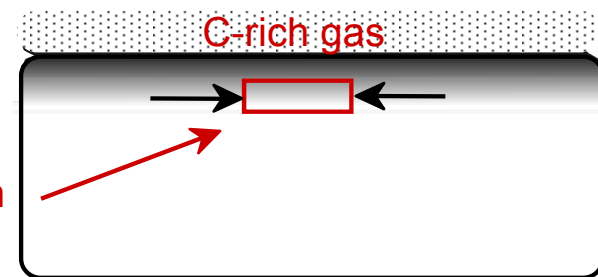
Improving Fatigue Life

1. Impose a compressive surface stress
(to suppress surface cracks from growing)

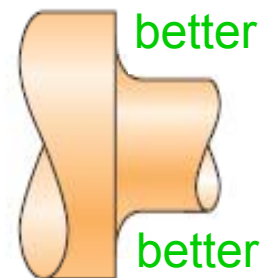
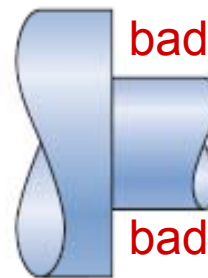
--Method 1: shot peening



--Method 2: carburizing

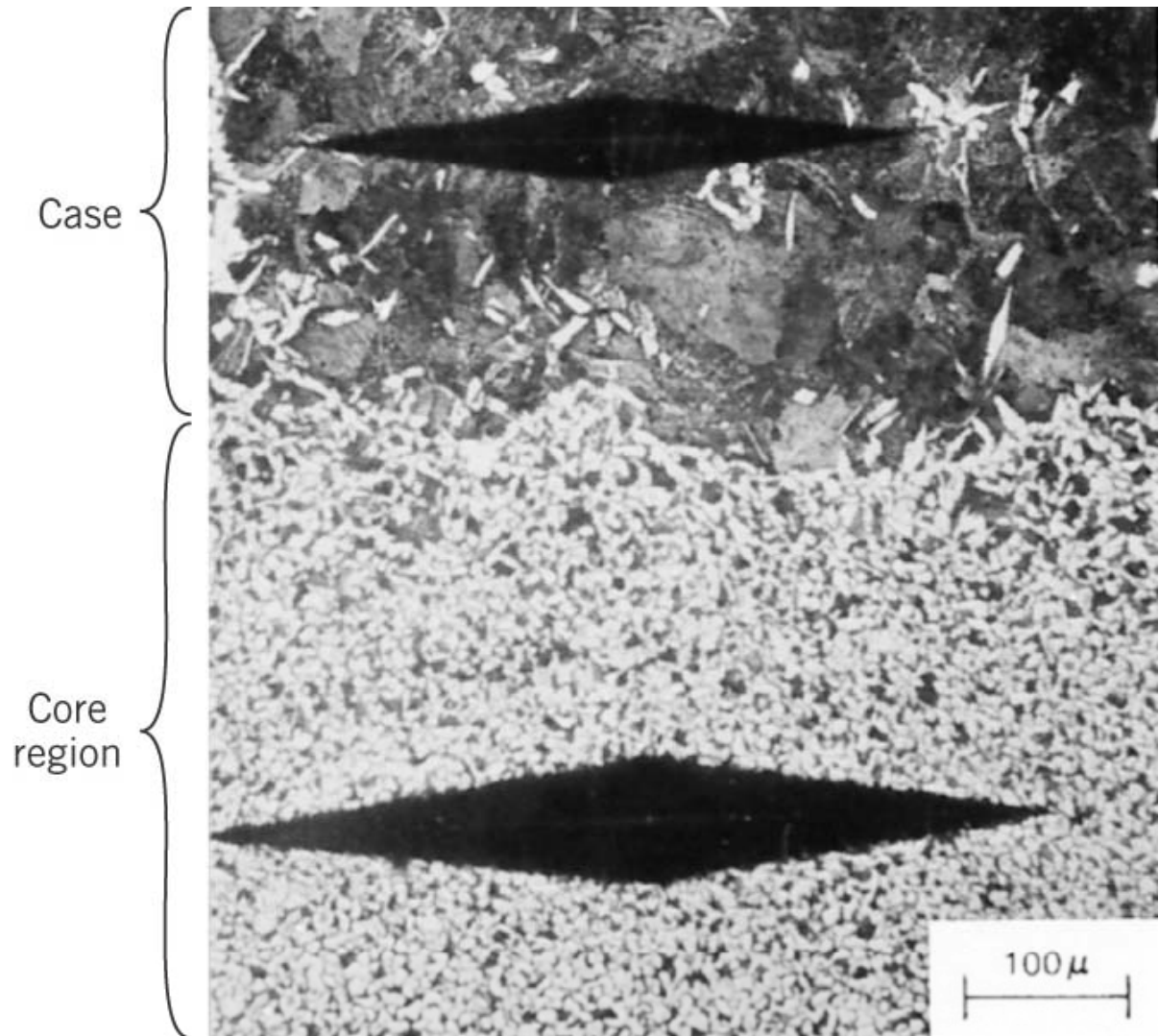


2. Remove stress concentrators.



Case Hardening

- Case hardening is a technique where both surface hardness and fatigue life are improved for steel alloys.
- Both core region and carburized outer case region are seen in image. Knoop microhardness shows case has higher hardness (smaller indent).
- A carbon or nitrogen rich outer surface layer (case) is introduced by atomic diffusion from the gaseous phase. The case is typically 1mm deep and is harder than the inner core material.



High Temperature - Creep

Temp



- Atoms move faster → **diffusion-controlled process**. This affects mechanical properties of materials.
- Greater mobility of dislocations (climb).
- Increased amount of vacancies.
- Deformation at grain boundaries.
- Metallurgical changes, i.e., phase transformation, precipitation, oxidation, recrystallisation.

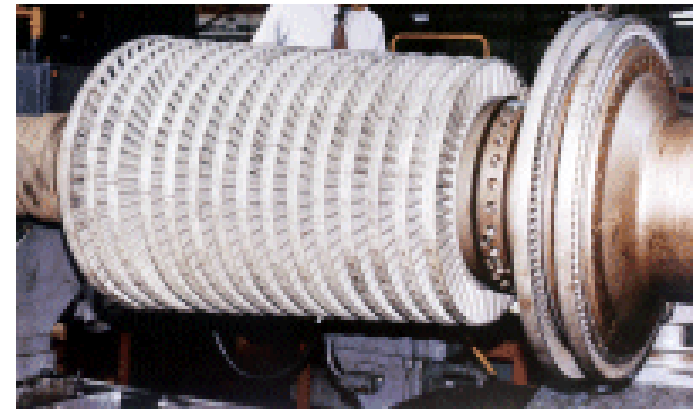


High temperature materials/alloys

- Improved high temperature strength.
- Good oxidation resistance.

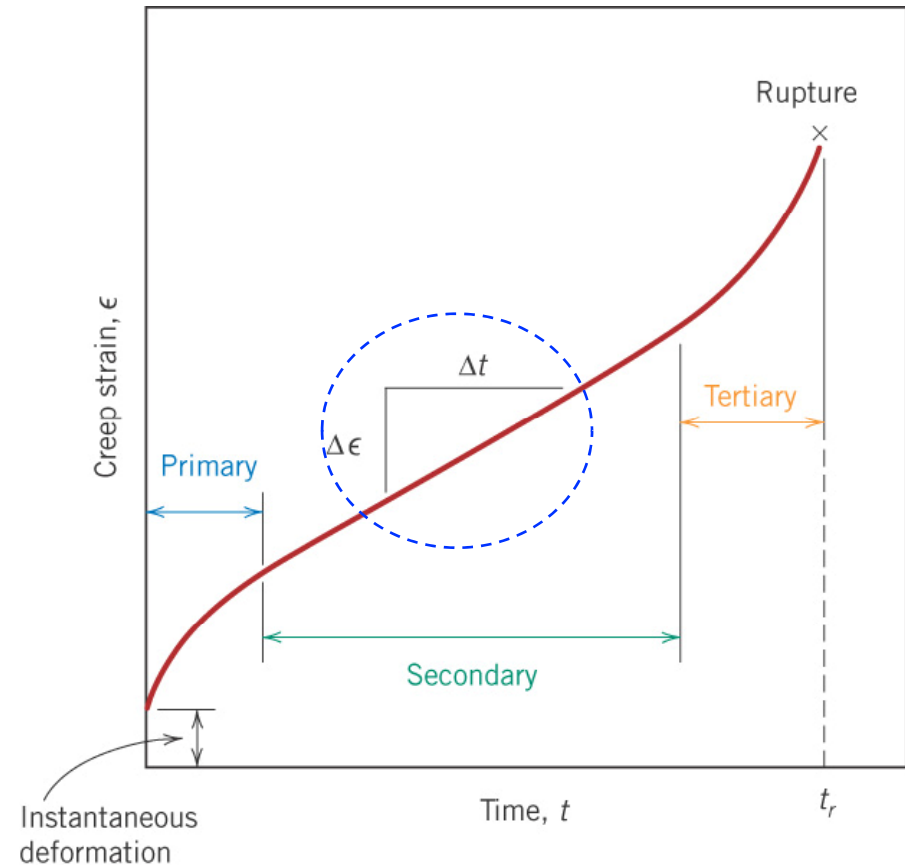
Creep

- Materials are often placed in service at elevated temperatures ($>0.4 T_m$) and exposed to static mechanical stresses.
- Examples are turbine **rotors** in jet engines and steam **generators** that experience centrifugal stresses and high pressure steam lines.
- **Creep** is time dependent, permanent deformation of the material when subjected to a constant load or stress.



Creep

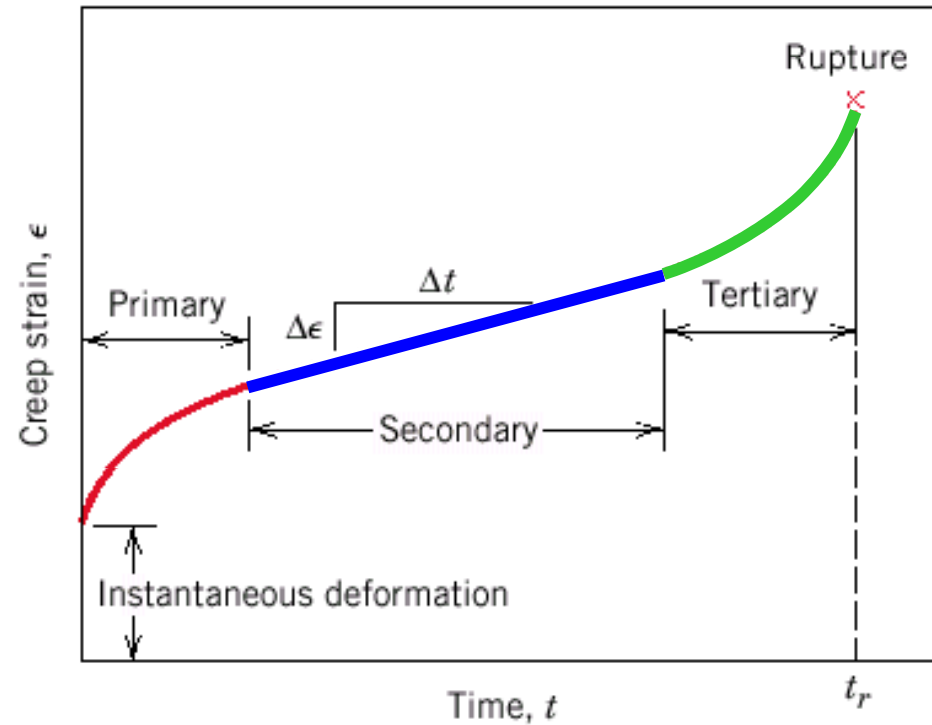
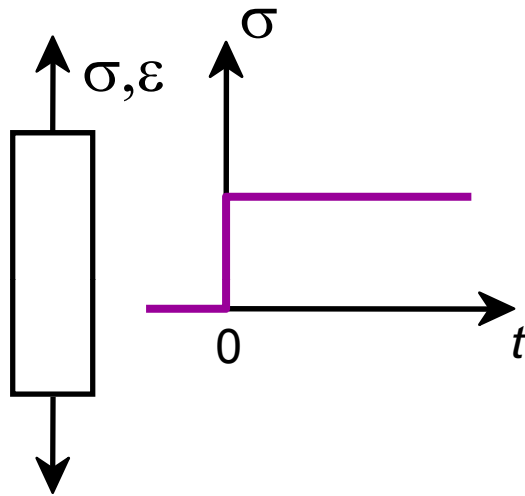
- A typical creep test consists of subjecting a specimen to a constant load or stress while maintaining constant temperature.
- Upon loading, there is instant elastic deformation. The resulting creep curve consists of 3 regions: **primary or transient** creep adjusts to the creep level (creep rate may decrease); **secondary creep**-steady state-constant creep rate, fairly linear region (strain hardening and recovery stage); **tertiary creep**, there is accelerated rate of strain until rupture (grain boundary separation, internal crack formation, cavities and voids).



Creep strain vs time at constant load and constant elevated temperature. Minimum creep rate (**steady-state creep rate**), is the slope of the linear segment in the secondary region. Rupture lifetime t_r is the total time to rupture.

Creep

Sample deformation at a constant stress (σ) vs. time

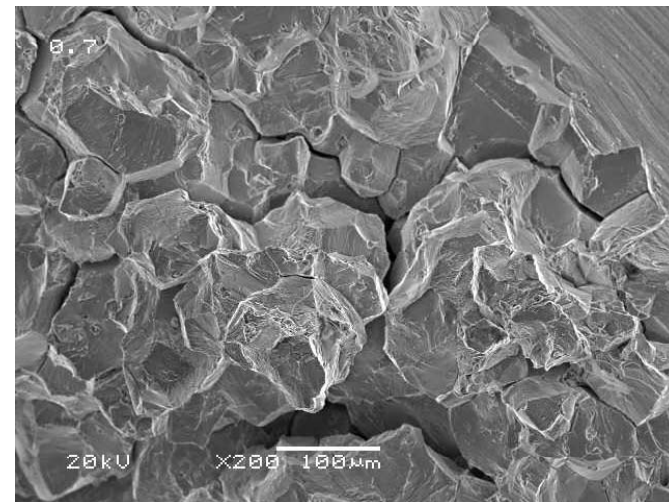
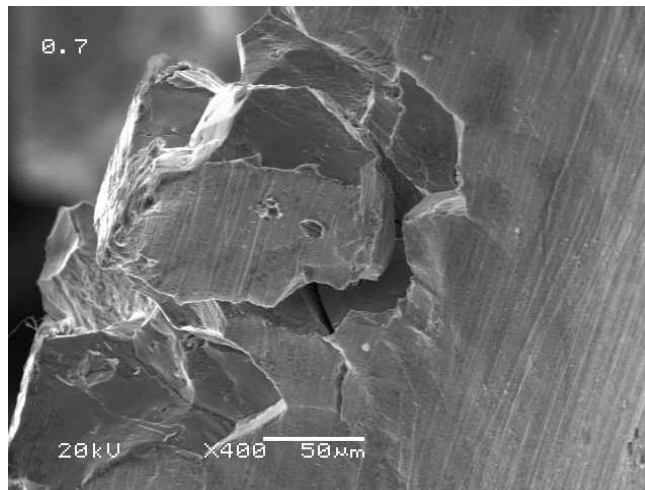
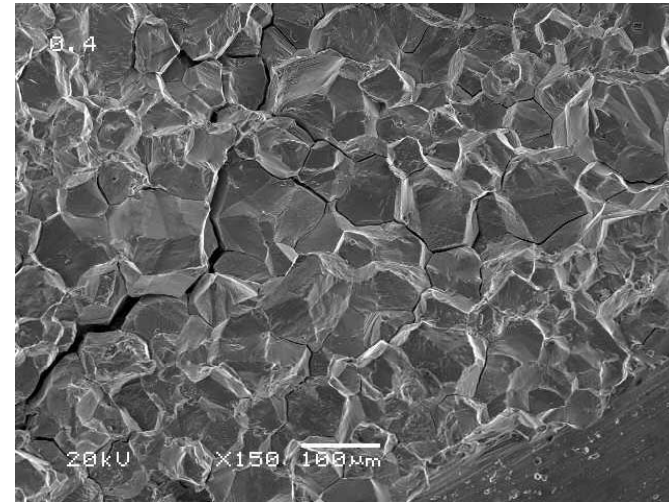
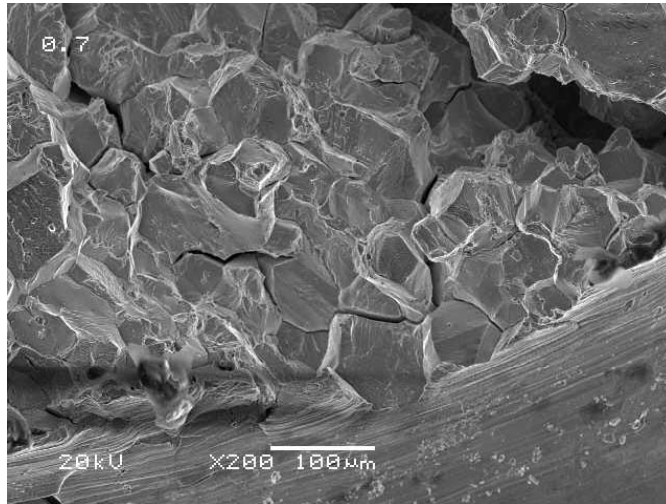


Primary Creep: slope (creep rate) decreases with time.

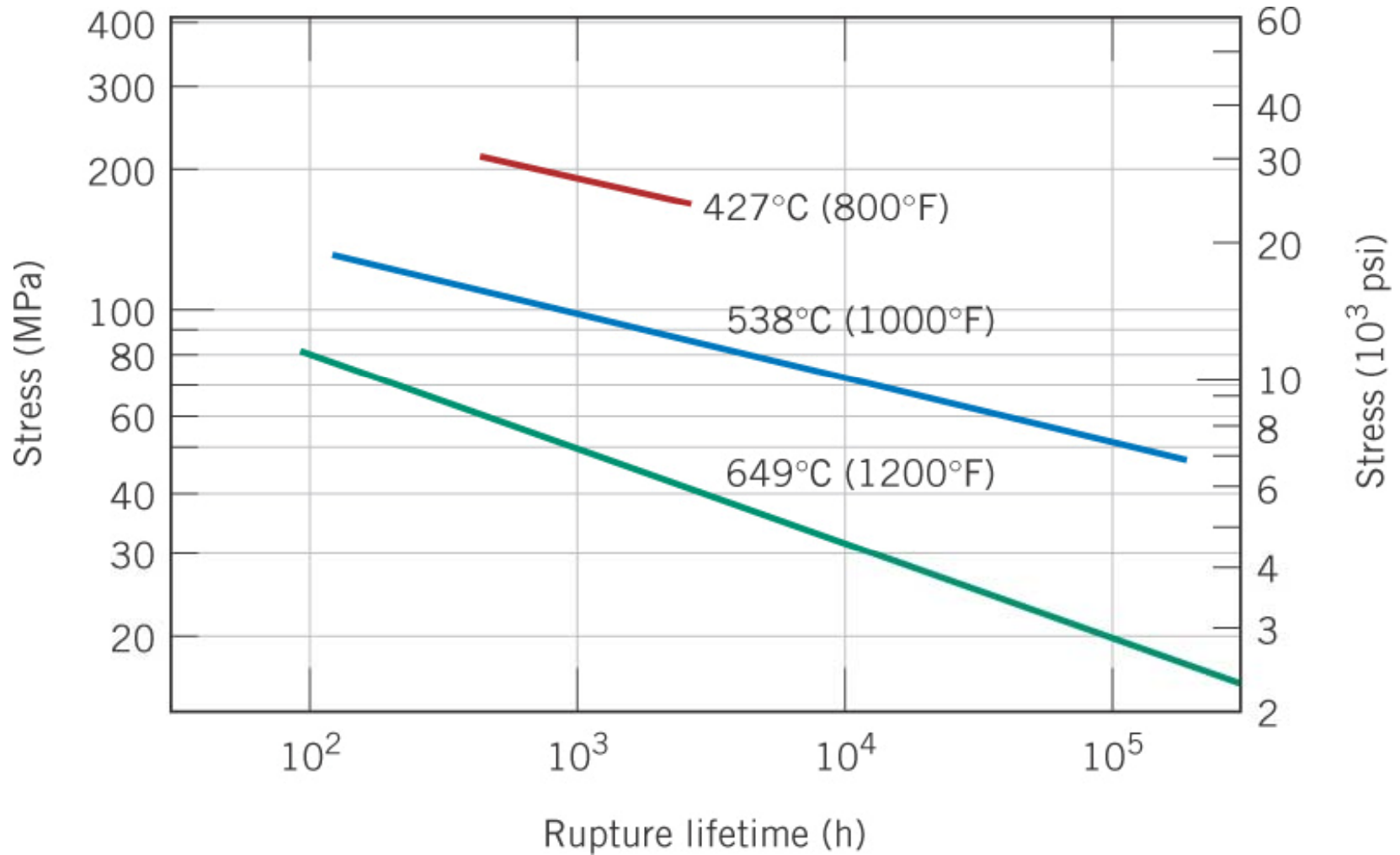
Secondary Creep: steady-state i.e., constant slope.

Tertiary Creep: slope (creep rate) increases with time, i.e. acceleration of rate.

Creep Failure



Creep



Dependence of creep strain rate on stress; stress versus rupture lifetime for a low carbon-nickel alloy at 3 temperatures.

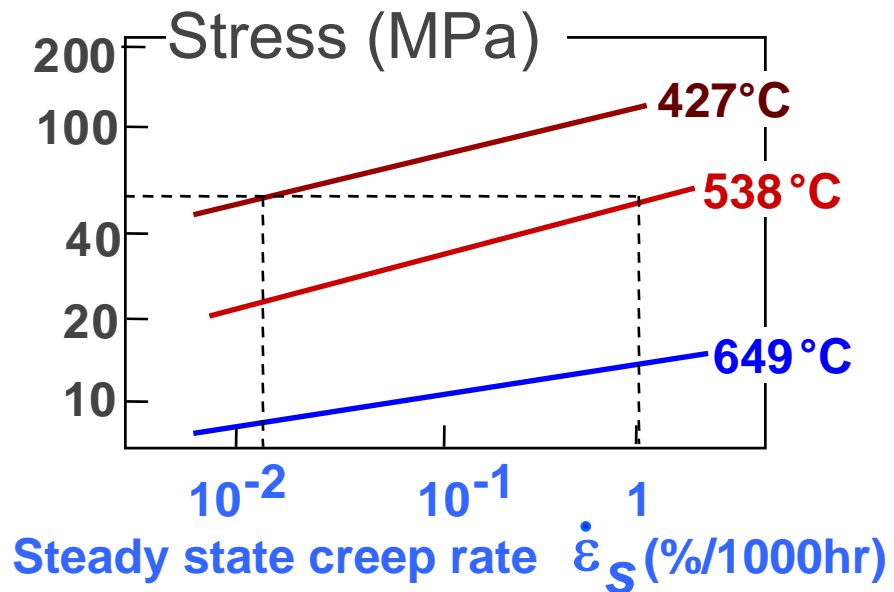
Secondary Creep

- Strain rate is constant at a given T, σ
 - strain hardening is balanced by recovery

$$\dot{\epsilon}_s = K_2 \sigma^n \exp\left(-\frac{Q_c}{RT}\right)$$

strain rate $\dot{\epsilon}_s$ (blue box)
 material const. K_2
 applied stress σ
 stress exponent (material parameter) n
 activation energy for creep (material parameter) Q_c (red box)

- Strain rate increases for higher T, σ



SUMMARY

- Engineering materials don't reach **theoretical strength**.
- **Flaws** produce **stress concentrations** that cause premature failure.
- Sharp corners produce large stress concentrations and premature failure.
- Failure type depends on T and stress:
 - for noncyclic σ and $T < 0.4 T_m$, failure stress decreases with:
 - increased maximum flaw size,
 - decreased T ,
 - increased rate of loading.
 - for cyclic σ :
 - cycles to fail decreases as $\Delta\sigma$ increases.
 - for higher T ($T > 0.4 T_m$):
 - time to fail decreases as σ or T increases.