

## **MAJOR REQUIREMENTS - OPTICAL FIBER EMITTER**

1. LIGHT O/P SHOULD BE HIGHLY DIRECTIONAL.
2. SOURCE SHOULD BE 'LINEAR' (MIN. DISTORTION AND NOISE)
3. SHOULD EMIT LIGHT AT WAVELENGTHS WHERE THE FIBER HAS LOW LOSSES & LOW DISPERSION.
4. SHOULD BE CAPABLE OF SIMPLE SIGNAL MODULATION OVER A WIDE BW (AUDIO TO GHz)
5. MUST COUPLE SUFFICIENT OPTICAL POWER INTO THE OFC.

6. SHOULD HAVE A NARROW LINEWIDTH (SO AS TO MINIMISE DISPERSION IN THE FIBER)

7. O/P SHOULD NOT BE TEMP DEPENDENT.

8. SOURCE SHOULD BE CHEAPER & RELIABLE.

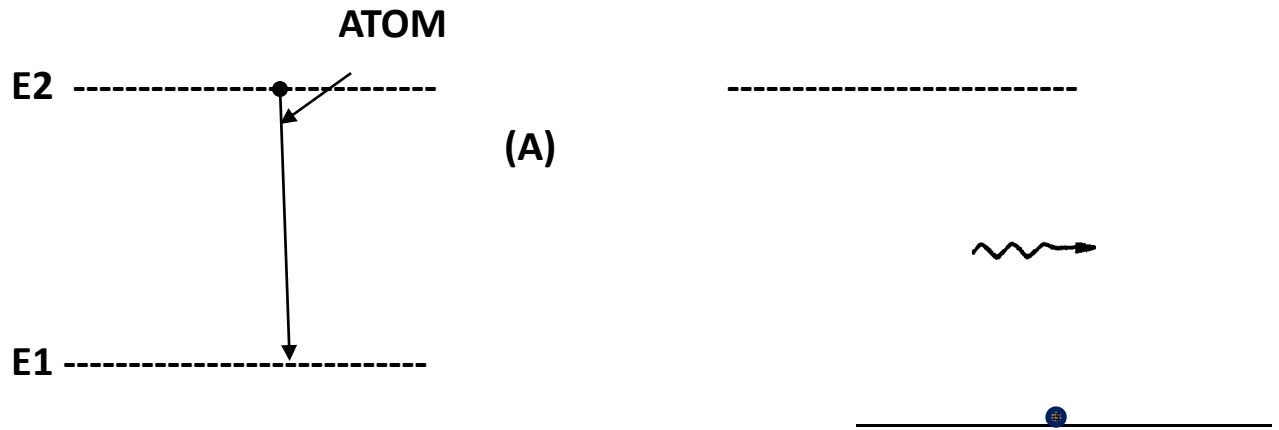
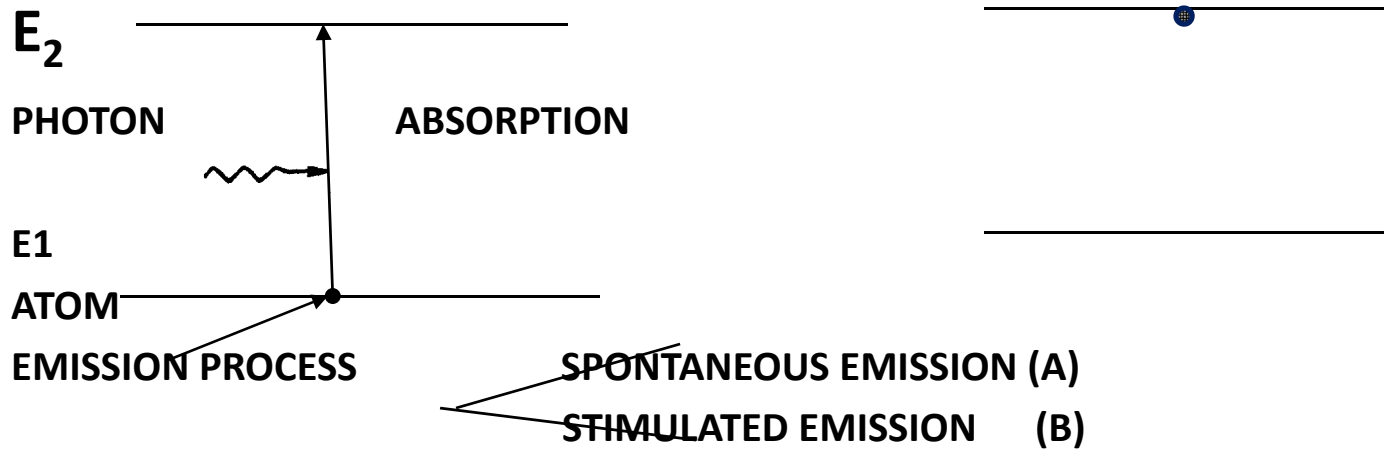
- **FIRST GENERATION OPTICAL SOURCES - 0.85  $\mu\text{m}$  (WAVELENGTH) .**

- **SECOND GENERATION OPTICAL SOURCES - 1.1 to 1.6  $\mu\text{m}$  (WAVELENGTH) •**

# ENERGY STATE DIAGRAM

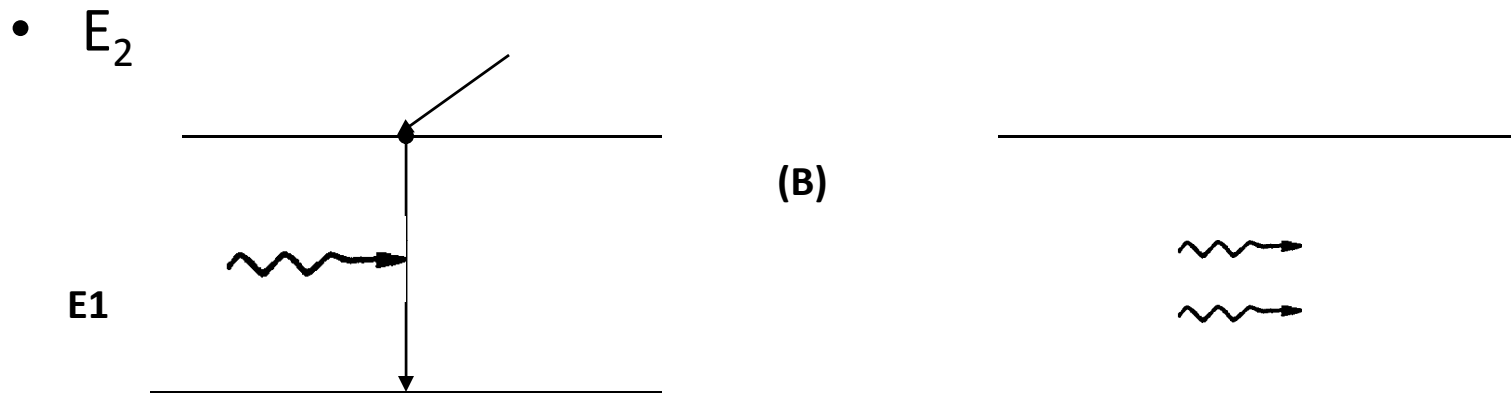
**INITIAL STATE**

**FINAL STATE**



- ATOM RETURNS TO LOWER ENERGY STATE IN AN ENTIRELY RANDOM MANNER (INCOHERENT LIGHT RADIATION)----LED !

ATOM



A PHOTON HAVING AN ENERGY EQUAL TO  $(E_2 - E_1)$  INTERACTS WITH THE ATOM (IN UPPER ENERGY STATE) CAUSING IT TO RETURN TO LOWER STATE WITH THE CREATION OF A SECOND PHOTON – (LASER !)

COHERENT RADIATION !



## OPTICAL SOURCE - 'LED'

- OPTICAL SOURCE CONVERTS ELECTRICAL ENERGY (CURRENT) INTO OPTICAL ENERGY (LIGHT).
- THREE TYPES OF OPTICAL SOURCES
  - WIDEBAND CONTINUOUS SPECTRA SOURCES (**INCANDESCENT LAMP**).
  - MONOCHROMATIC INCOHERENT SOURCES (**LEDs**)
  - MONOCHROMATIC COHERENT SOURCES (**LASERS**).

### **LED'S ADVANTAGES :-**

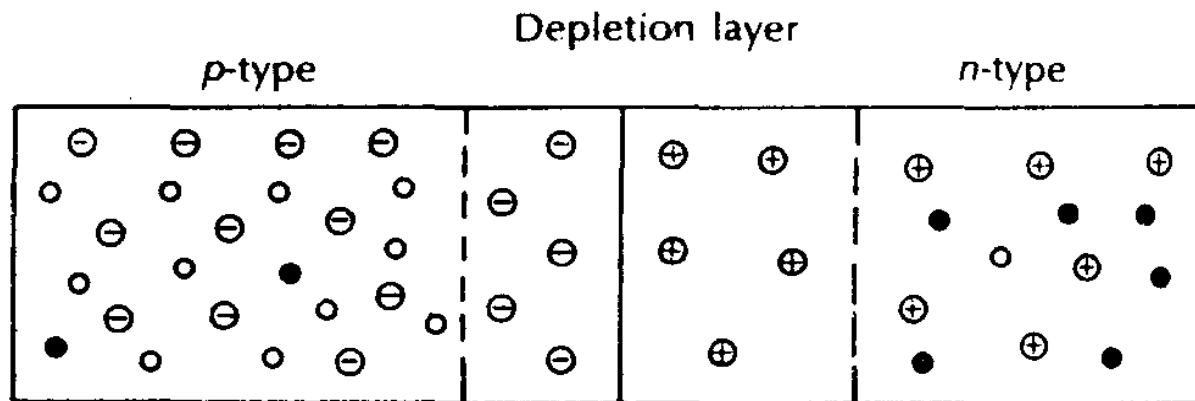
- SIMPLE CONSTRUCTION & OPERATION
- LOWER COST
- TROUBLE FREE LIFE (HIGH RELIABILITY)
- . LESS TEMP DEPENDANCE
- LINEARITY

### **DISADVANTAGES:-**

- LOWER OPT POWER CAN BE COUPLED INTO OFC
- LOWER MODULATION BANDWIDTH
- HARMONIC DISTORTION

**HOWEVER,LEDs CONTINUE TO REMAIN A PROMINENT OPTICAL FIBER COMMUNICATION SOURCE FOR MANY SYSTEM APPLICATIONS.**

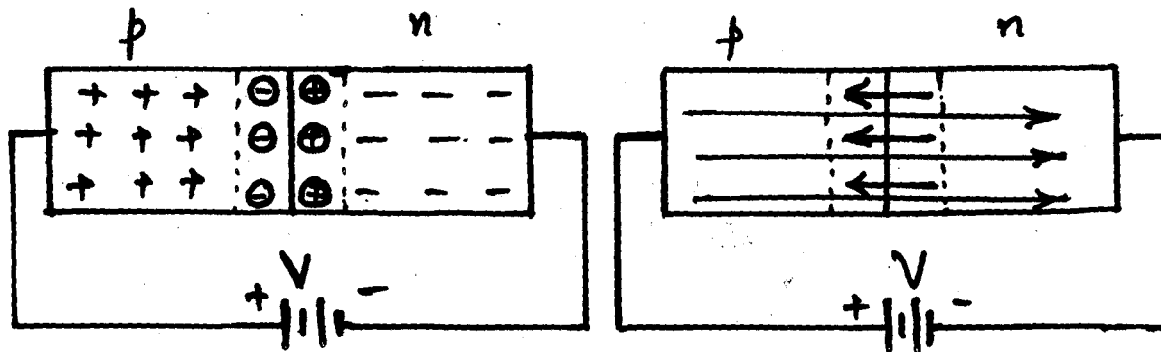
# OPT. EMISSION FROM SEMICONDUCTOR THE P-N JUNCTION



Impurities and charge carriers at the PN junction

BARRIER POTENTIAL : 0.3V (Ge), 0.7V (Si) AT 25<sup>0</sup>C

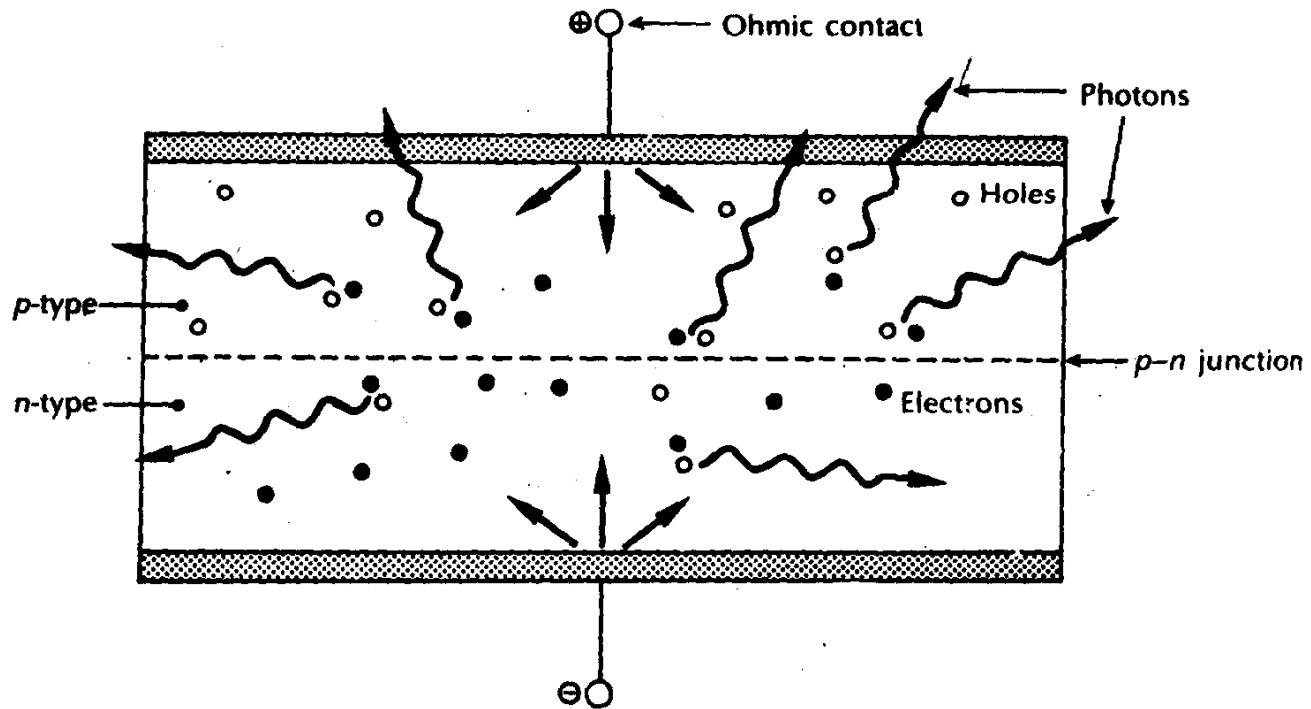
# FORWARD BIAS



- THE APPLIED FIELD OPPOSES THE DEPLETION LAYER FIELD .
- THUS IT PUSHES ELECTRONS & HOLES TOWARDS THE JUNCTION.
- EDGES OF DEPLETION LAYER GET DE-IONISED .
- THIS NARROWS THE DEPLETION LAYER.
- THUS GREATER THE EXTERNAL VOLTAGE NARROWER THE DEPLETION LAYER.
- **RECOMBINATION BETWEEN ELECTRONS AND HOLES OCCUR AROUND THE JUNCTION.**



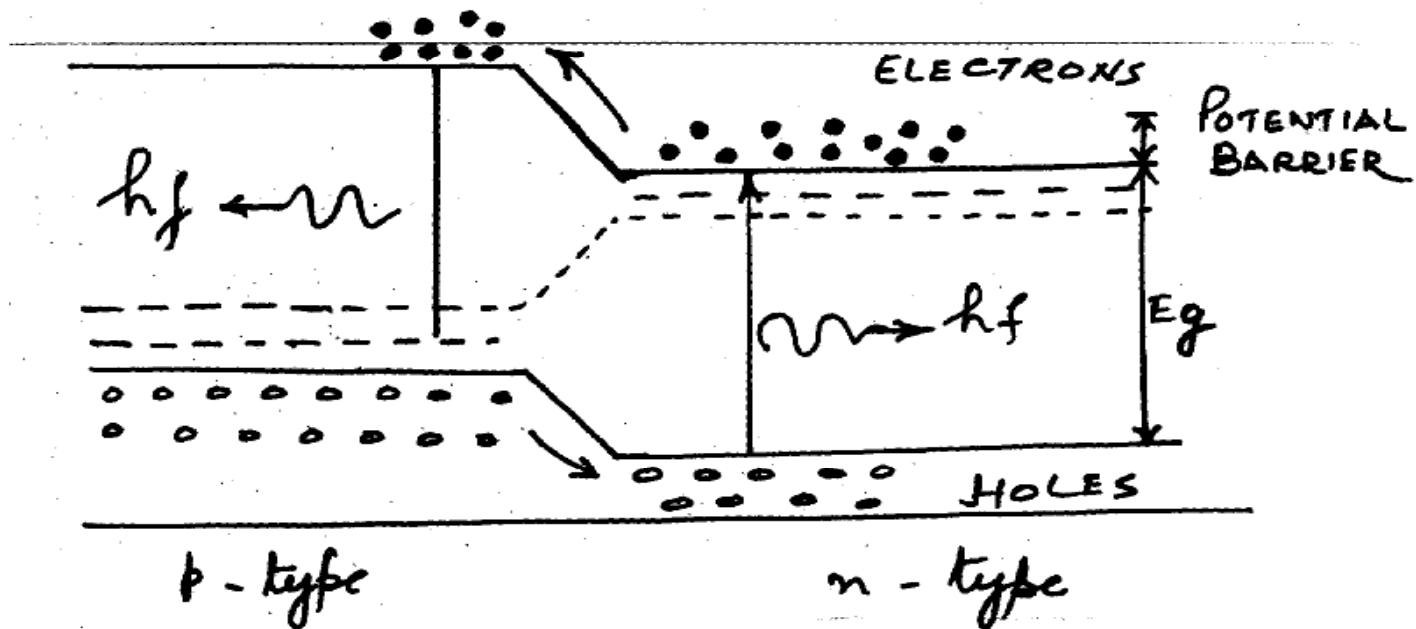
## CARRIER COMBINATION GIVING SPONTANEOUS EMISSION OF LIGHT



An illustration of carrier recombination giving spontaneous emission of light in a p—n junction diode.

THE AVERAGE TIME THE MINORITY CARRIER REMAINS IN A FREE STATE BEFORE RECOMBINATION IS SHORT,  $10^{-8}$  TO  $10^{-10}$  SEC. (MINORITY CARRIER LIFETIME)

## PRINCIPLE OF OPERATION - LED



PN JUNCTION WITH FORWARD BIASING

- **INCREASED CONCENTRATION OF MINORITY CARRIERS IN THE OPPOSITE TYPE REGION IN FORWARD BIASED P-N DIODE LEADS TO RECOMBINATION OF CARRIERS.**
- ENERGY RELEASED BY ELECTRON HOLE RECOMBINATION IS APPROX. EQUAL TO BAND GAP ENERGY  $E_g$ .
- **ENERGY IS RELEASED WITH THE CREATION OF A PHOTON.**  
 $E_g = hf = hc/\lambda$  WHERE  $h = 6.626 \times 10^{-34}$  J (PLANCK'S CONSTANT)

**THIS SPONTANEOUS EMISSION OF LIGHT FROM DIODE IS CALLED- ELECTROLUMINESCENCE.**

## LED'S POWER & EFFICIENCY

INTERNAL QUANTUM  $\eta = \frac{\text{NO OF PHOTONS GENERATED}}{\text{NO OF ELECTRONS INJECTED}}$

RECOMBINATION ~~NON-RADIATIVE~~ (PHOTON IS GENERATED)  
(ENERGY RELEASED IN THE FORM OF HEAT)

INTERNAL QUANTUM  $\eta = \frac{\text{RADIATIVE RECOMBINATION RATE}}{\text{TOTAL RECOMBINATION RATE}}$

$$= \frac{r_r}{r_r + r_{nr}} = \frac{r_r}{r_t}$$

NON-RADIATIVE RECOMBINATION TAKES PLACE WITHIN THE STRUCTURE DUE TO CRYSTALLINE IMPERFECTIONS AND IMPURITIES GIVING AN EFFICIENCY OF 50% (MAX)

- **LED'S POWER & EFFICIENCY (contd)**

- THE ENERGY RELEASED BY THIS ELECTRON – HOLE RECOMBINATION IS APP. EQUAL TO BANDGAP ENERGY  $E_g = hf$ .

- LET  $\Delta n =$  EXCESS DENSITY OF ELECTRONS IN p – TYPE MATERIAL .

$\Delta p =$  EXCESS DENSITY OF HOLES IN n- TYPE MATERIAL.

$\Delta n = \Delta p$  (FOR CHARGE NEUTRALITY)

## RATE = n FOR CARRIER RECOMBINATION

$$d/dt (\Delta n) = J/ed - \Delta n/\tau \quad (\text{m}^{-3}\text{s}^{-1})$$

At equilibrium, rate of change of density = 0

$$\text{or } J/ed = \Delta n/\tau \quad \text{or } \Delta n = J\tau/ed \quad (\text{m}^{-3}) \quad (1)$$

=n(1) GIVES STEADY STATE ELECTRON DENSITY WHEN A  
CONSTANT CURRENT IS FLOWING INTO JUNCTION

AT STEADY STATE, TOTAL NO OF CARRIER RECOMBINATIONS PER  
SECOND, =  $r_t = J/ed = r_r + r_{nr}$

## RATE = n FOR CARRIER RECOMBINATION

- $\Delta n = \Delta n (0) e^{-t/\tau}$
- WHERE  $\Delta n (0)$  = Initial injected excess electron density :

$\tau$  = total carrier recombination life time.

At equilibrium (constant current flows into junction diode)

TOTAL RATE (carrier generation) = EXT SUPPLIED + THERMALLY GENERATED

Let  $J$  = CURRENT DENSITY (amp/m<sup>2</sup>)

=  $J/ed$  = ELECTRONS PER CUBIC METRE PER SEC.

(where  $d$  = thickness of recombination region)

FURTHER,  $R_t$  = total number of recombinations per sec =  $i/e$  (  $i$  = forward bias current)

**LED INTERNAL QUANTAM EFFICIENCY**

$$\eta_{\text{int}} = \frac{\text{Radiative Recombination rate}}{\text{Total recombination rate}} = \frac{r_r}{r_t} = \frac{r_r}{r_r + r_{nr}}$$

$$= R_r / R_t$$

Or  $R_r = \eta_{\text{int}} \times R_t = \eta_{\text{int}} \times i/e$   
**= total no of photons generated per sec.**

ENERGY IN EACH PHOTON  $E_g = hf$  joules



## OPT POWER GENERATED BY LED ( $P_{int}$ )

= No of photons generated x energy /photon

=  $\eta_{int} \times i/e \times hf$  Watts

$$P_{int} = \eta_{int} \times hci/e\lambda$$

**NOW**  $\tau_r$  = RADIATIVE MINORITY CARRIER LIFE TIME.

$$= \Delta n / r_r = \frac{\text{electrons /m}^3}{\text{electrons /m}^3 / \text{sec.}}$$

$$\tau_{nr} = \Delta n / r_{nr}$$

$$\eta_{int} = r_r / (r_r + r_{nr})$$

$$\eta_{int} = r_r / (r_r + r_{nr}) = 1 / (1 + (r_{nr} / r_r)) = 1 / (1 + (\tau_r / \tau_{nr}))$$

$$r_{nr} / r_r = \Delta n / \tau_{nr} \times \tau_r / \Delta n = \tau_r / \tau_{nr}$$

Hence  $\eta_{int} = 1 / (1 + (\tau_r / \tau_{nr}))$

$$\begin{aligned}
 \text{Also } \tau &= \text{Total recomb.life time} = \Delta n / r_t \\
 &= \Delta n / (r_r + r_{nr}) = \Delta n / (\Delta n / \tau_r) + (\Delta n / \tau_{nr}) \\
 &= 1 / (1 / \tau_r) + (1 / \tau_{nr})
 \end{aligned}$$

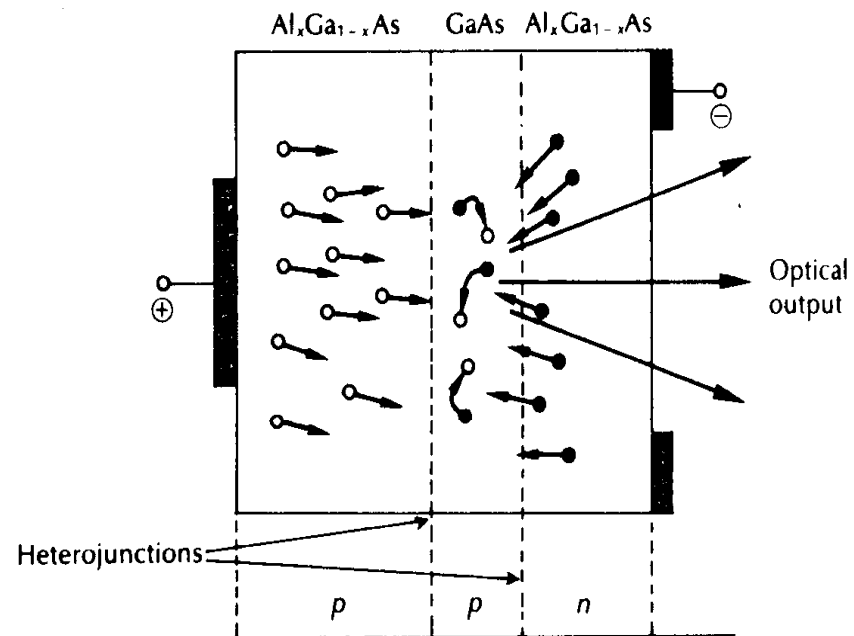
$$1 / \tau = 1 / \tau_r + 1 / \tau_{nr}$$

$$\begin{aligned}
 \text{Further } \eta_{\text{int}} &= r_r / (r_r + r_{nr}) \\
 &= r_r / r_t
 \end{aligned}$$

$$\begin{aligned}
 &= \frac{\Delta n / \tau_r}{\Delta n / \tau} = \tau / \tau_r \\
 &(\Delta n / \tau)
 \end{aligned}$$

$$\text{Hence } \eta_{\text{int}} = \tau / \tau_r$$

# THE DOUBLE HETEROJUNCTION LED



Layered Structure With Applied Forward Bias

# THE DOUBLE HETROJUNCTION LED

- p- TYPE GaAs IS SANDWITCHED BETWEEN A p-TYPE Al Ga As AND AN n-TYPE Al Ga As .
- **ON APPLICATION OF FORWARD BIAS**
- ELECTRONS FROM n TYPE ARE INJECTED THR' p-n JUNCTION, INTO p TYPE GaAs LAYER.
- THESE MINORITY CARRIERS RECOMBINE WITH MAJORITY CARRIERS (HOLES).
- PHOTONS ARE PRODUCED WITH ENERGY CORRESP TO BAND GAP ENERGY OF p- TYPE GaAs LAYER.
- THE INJECTED ELECTRONS ARE INHIBITED FROM DIFFUSING INTO p – TYPE Al Ga As LAYER BECAUSE OF POTENTIAL BARRIER PRESENTED BY p-p HETROJUNCTION

## THE DOUBLE HETEROJUNCTION LED(contd)

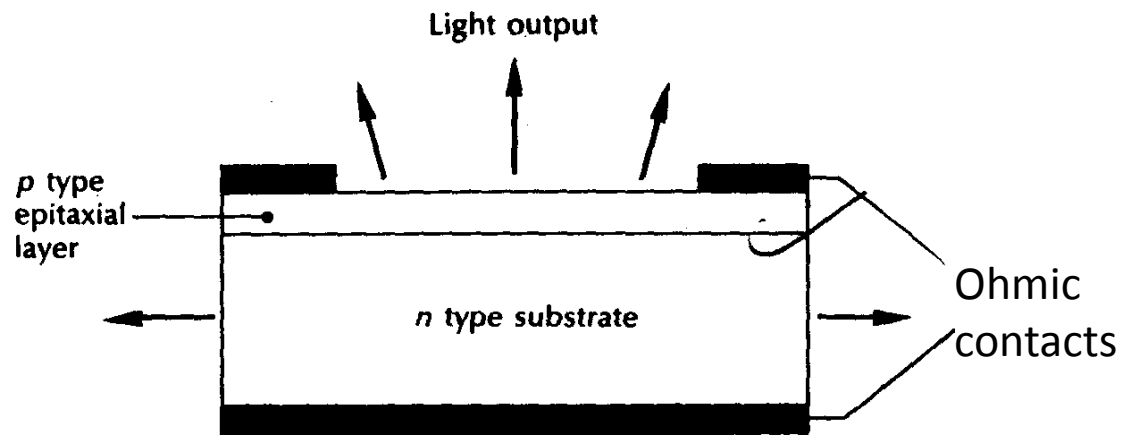
- THUS ELECTRO LUMINESCENCE OCCURS ONLY IN GaAs LAYER PROVIDING GOOD INTERNAL QUANTUM EFFICIENCY AND' HIGH RADIANCE EMISSION.
- **THE DH STRUCTURE IS MOST EFFICIENT INCOHERENT SOURCE FOR OPT.FIBER COMM.**

# LED STRUCTURES

## FIVE MAJOR TYPES OF LED STRUCTRE

- PLANNAR LED'S
- DOME LED'S
- SURFACE EMITTER LED'S
- EDGE EMITTER LED'S
- SUPER LUMINESCENT LED'S

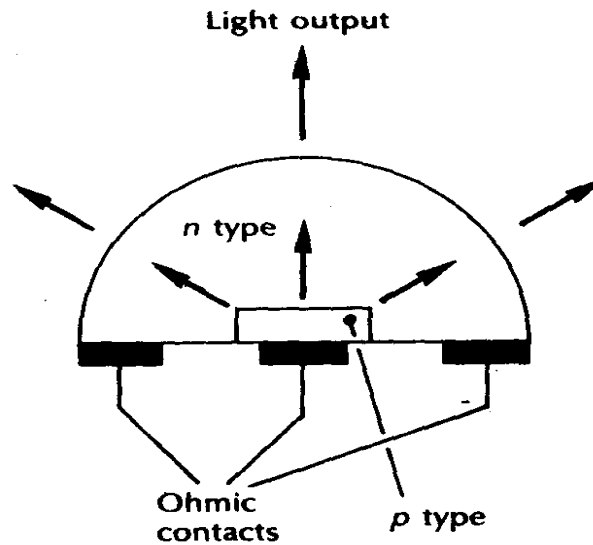
### PLANAR LED



The structure of a planar LED showing the emission of light from all surfaces.

- P TYPE DIFFUSION OCCURS INTO N TYPE SUBSTRATE
- FORWARD CURRENT FLOWS THR' JUNCTION AND DEVICE EMITS LIGHT .
- HOWEVER, RADIANCE IS LOW (light emitted from entire surface)

# DOME LED



- DIA OF DOME IS SO CHOSEN TO MAXIMISE AMOUNT OF INTERNAL EMISSION REACHING THE SURFACE (WITHIN CRITICAL ANGLE OF GaAs- AIR INTERFACE).
- HIGHER EXT EFFICIENCY THAN PLANAR LED
- **DOME SIZE IS FAR GREATER THAN THE ACTIVE RECOMBINATION AREA . SO EFFECTIVE EMISSION AREA IS GREATER ,THEREBY REDUCING THE RADIANCE.**

## **SURFACE EMITTER LED (SLED)**

- **GIVES HIGH RADIANCE**

- DUE TO LOW INTERNAL ABSORPTION

- HIGHER REFLECTION COEFFICIENT AT BACK CRYSTAL FACE (GIVING GOOD FORWARD RADIANCE)

- POWER COUPLED INTO MULTIMODE STEP INDEX FIBER.

$$P_c = \pi(1-r)A R_D (NA)^2 \text{ — (1)}$$

r-FRESNEL COEFFICIENT AT FIBER SURFACE

A-EMISSION AREA OF THE SOURCE

$R_D$ - RADIANCE OF THE SOURCE



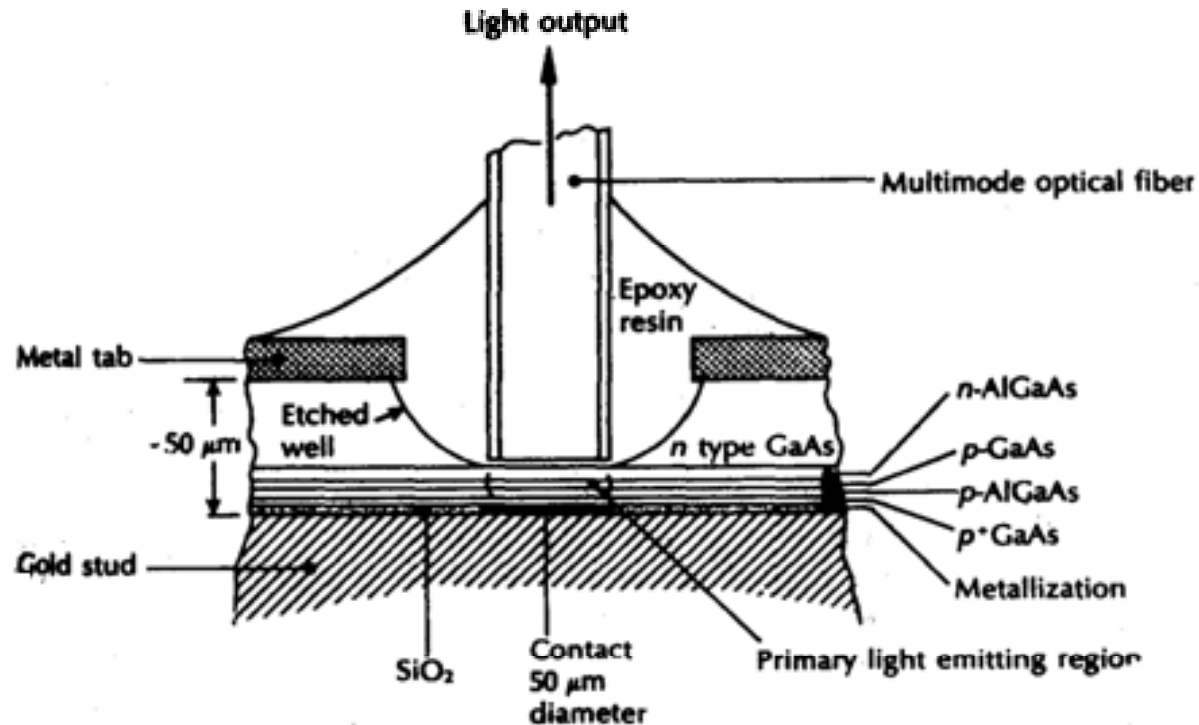
POWER COUPLED ALSO DEPENDS UPON

- **DISTANCE AND ALIGNMENT BETWEEN EMISSION AREA & FIBER**
- **SLED EMISSION PATTERN**
- **MEDIUM BETWEEN EMITTING AREA & FIBER**
  
- **DOUBLE HETEROJUNCTION LED SURFACE EMITTERS GIVE MORE COUPLED OPTICAL POWER THAN GIVEN BY  $\eta_{ext}$**

## SLED (contd)

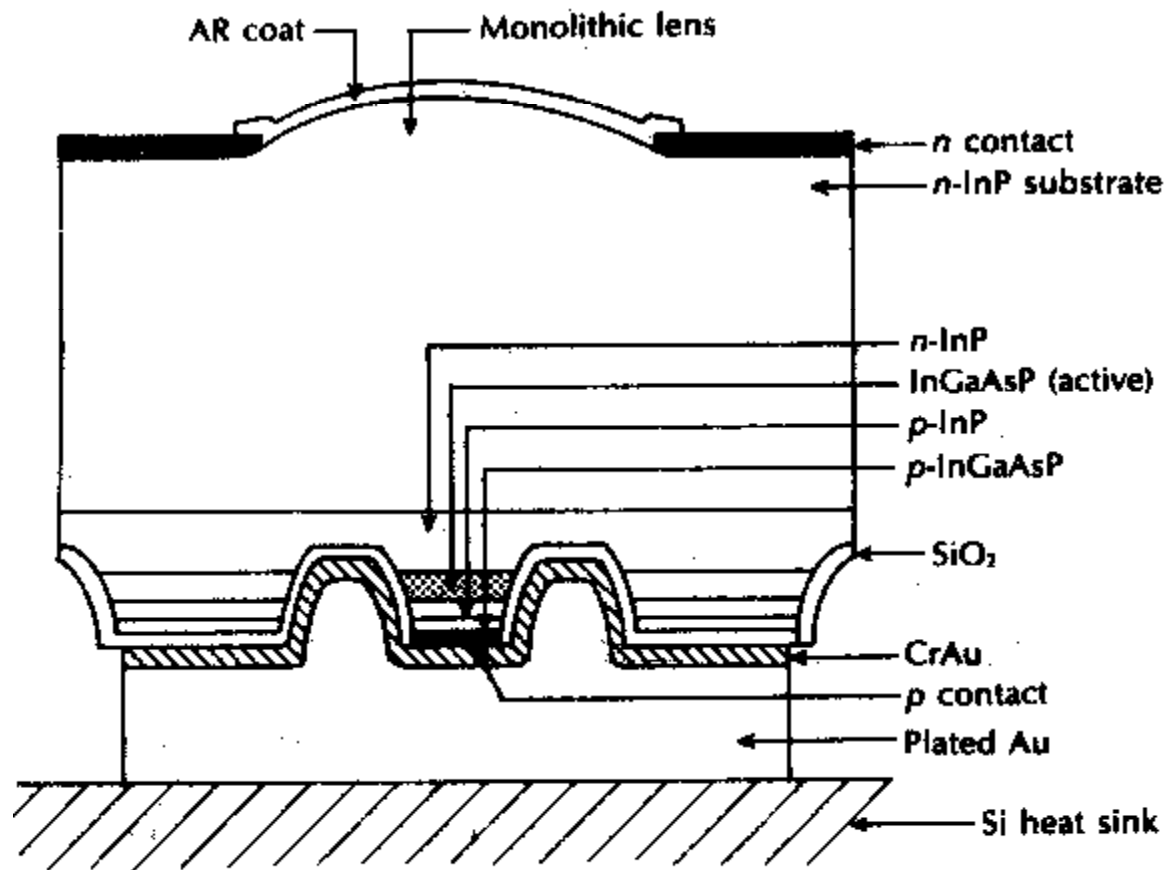
- MUCH OF THE LIGHT COUPLED INTO A MM FIBER FROM A LED IS LOST WITHIN A FEW HUNDRED METRES.
- HENCE **MORE POWER IS COUPLED INTO SHORTER LENGTH THAN LONGER LENGTH.**
- **THE SLED'S SUFFER FROM CURRENT SPREADING RESULTING IN REDUCED CURRENT DENSITY & EFFECTIVE EMISSION AREA GREATER THAN CONTACT AREA.**

## Al Ga As DH SURFACE EMITTING LED (0.8-0.9 $\mu\text{m}$ WAVE LENGTH)



The structure of an AlGaAs DH surface-emitting LED (Burrus type)

- INTERNAL ABSORPTION OF THIS DEVICE IS LOW DUE TO LARGE BAND GAP CONFINING LAYERS.
- THE ADDITION OF EPOXY RESIN IN THE ETCHED WELL TENDS TO REDUCE THE REFRACTIVE INDEX MISMATCH AND INCREASE THE EXTERNAL POWER EFFICIENCY OF THE DEVICE.

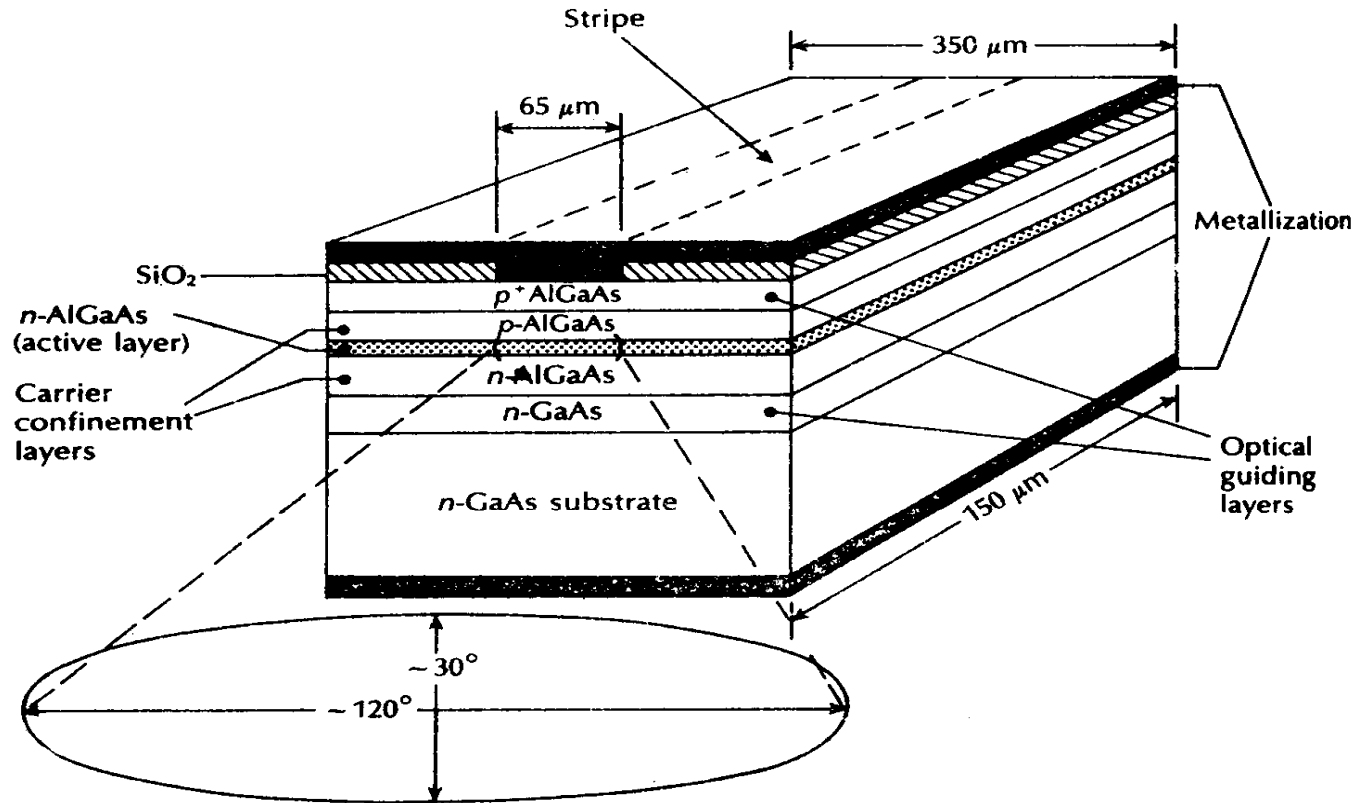


Small area InGaAsP mesa-etched surface-emitting LED structure

## In Ga As P MESA ETCHED SELED STRUCTURE(contd)

- **MESA STRUCTURE** (mesa dia 20 to 25  $\mu\text{m}$  at the active layer) REDUCES THE CURRENT SPREADING
- WAVE LENGTH = 1.3  $\mu\text{m}$
- THE STRUCTURE IMPROVES THE COUPLING  $\eta$  DUE TO FORMATION OF INTEGRAL LENS AT EXIT FACE.
- **TYPICAL DATA** : WITH A DRIVE CURRENT OF 50 mA, IT COUPLES 2  $\mu\text{w}$  POWER INTO A SINGLE MODE FIBER.
- COUPLING  $\eta$  UPTO 15% CAN BE ACHIEVED WITH OPTIMISED DEVICES.

# EDGE EMITTING LED'S (ELED)

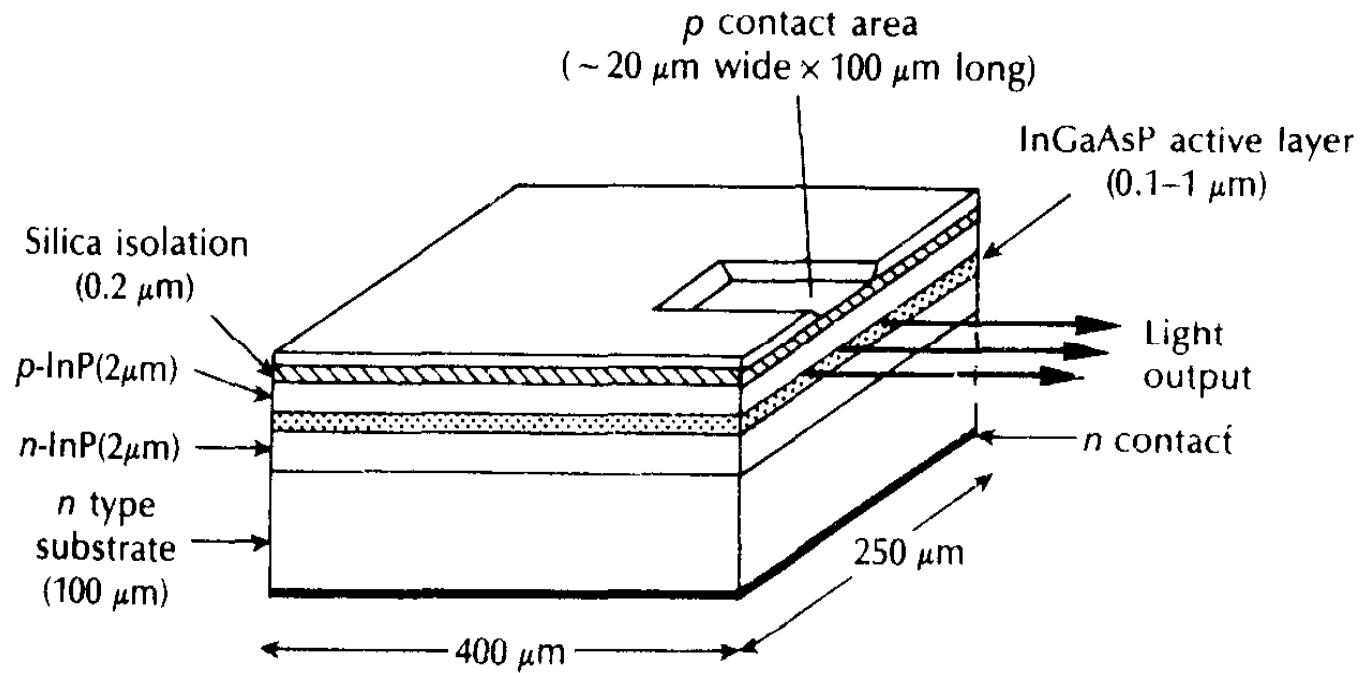


Stripe Geometry DH AlGaAs Edge Emitting LED

## ELED (contd)

- ACTIVE LAYER (50 TO 100  $\mu\text{m}$ ) WITH TRANSPARENT GUIDING LAYERS REDUCES SELF ABSORPTION IN THE ACTIVE LAYER.
- O/P WITH HALF POWER WIDTH OF  $30^\circ$  &  $120^\circ$
- MOST OF LIGHT EMISSION IS AT ONE END FACE ONLY
- EDGE EMITTERS COUPLE MORE OPTICAL POWER INTO LOW NA  $< 0.3$  THAN SELED, AND OPPOSITE IS TRUE FOR NA  $> 0.3$ .
- **COUPLING  $\eta$  IS 3.5 to 6 TIMES THAN SELED.**
- USE OF LENS COUPLING INCREASES COUPLING  $\eta$  ( 5 TIMES).
- EDGE EMITTERS ALSO **GIVE BETTER MODULATION BW** (HUNDREDS OF MHz) THAN COMPARABLE SELED WITH THE SAME DRIVE LEVEL.
- ELED'S HAVE **LESSER SPECTRAL LINE WIDTH** THAN SELED.

# TRUNCATED STRIPE In Ga As P EDGE EMITTING LED

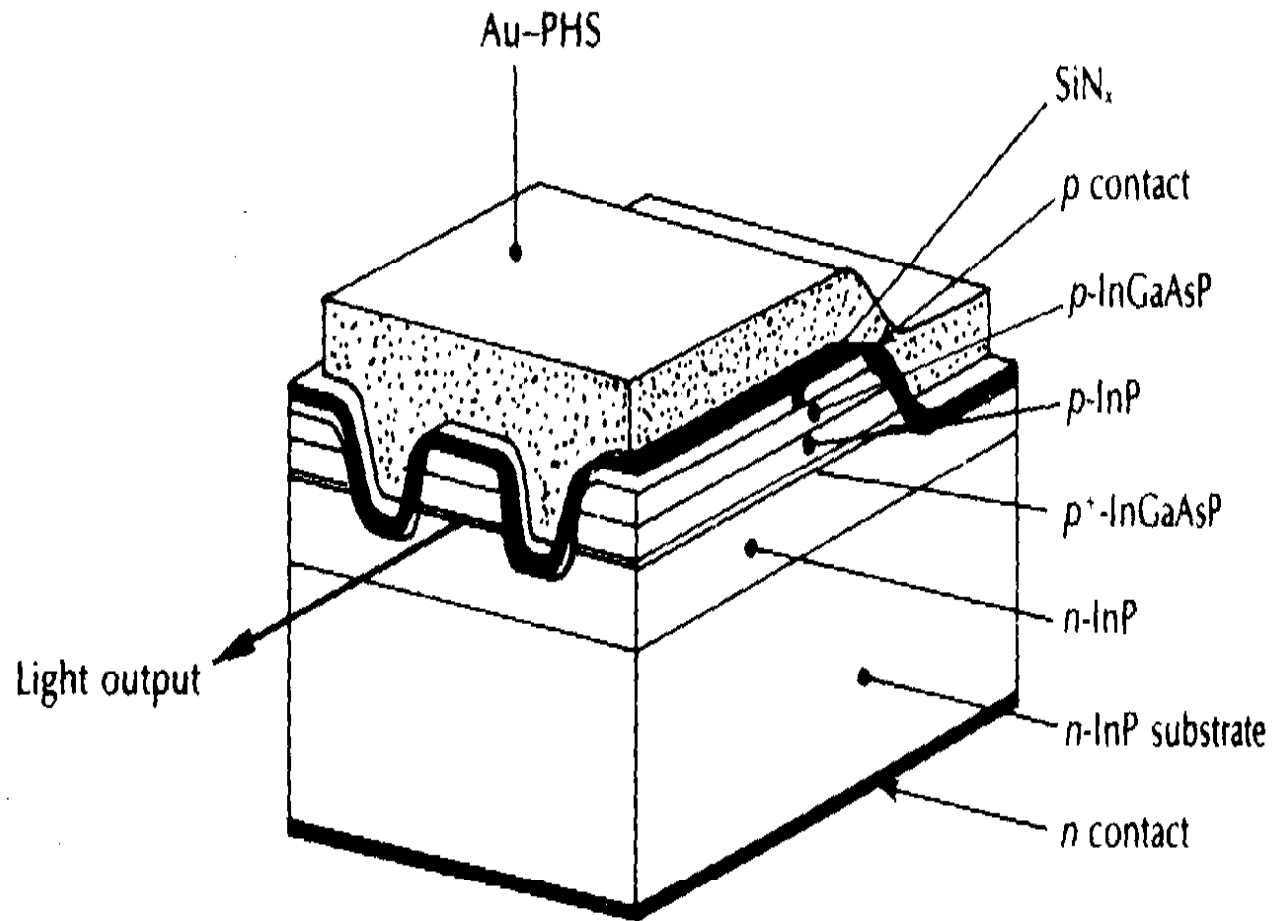


Truncated Stripe InGaAsP Edge Emitting LED



- **TRUNCATED STRIPE In Ga As P EDGE EMITTING LED ( Contd )**
- OPERATING WAVE LENGTH =  $1.3 \mu\text{m}$ .
- THE DEVICE IS DH EDGE EMITTING LED HAVING RESTRICTED LENGTH ,STRIPE GEOMETRY p – CONTACT ARRANGEMENT.
- THE EXTERNAL EFFICIENCY OF THE ELED IS HIGHER DUE TO LESSER INTERNAL ABSORPTION OF CARRIERS.
- SILICA LAYER GIVES THE ISOLATION BETWEEN THE p TYPE LAYERS.
- STRIPE  $100 \mu\text{m}$  LENGTH  
 $20 \mu\text{m}$  WIDTH

## HIGH SPEED In Ga As EDGE EMITTING LED'S



Mesa Structure High Speed LED

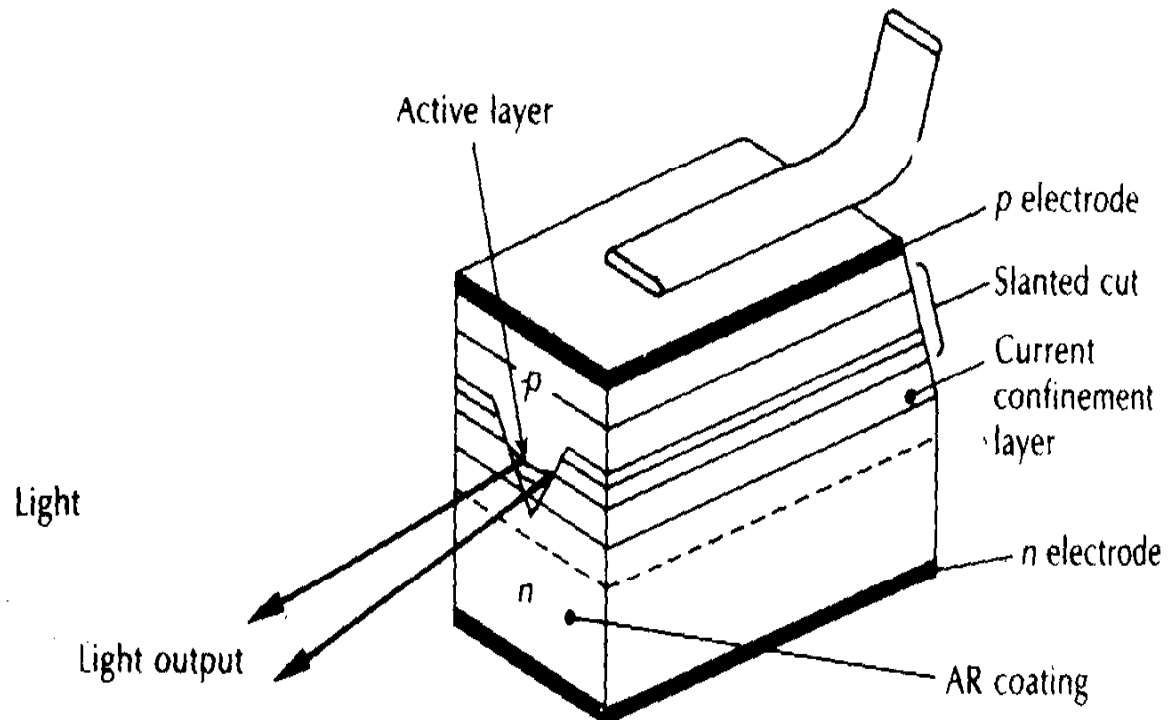
## HIGH SPEED In Ga As EDGE EMITTING LED'S

- MESA STRUCTURE (8  $\mu\text{m}$  WIDTH x 150  $\mu\text{m}$  LENGTH FOR CURRENT CONFINEMENT).
- TILTED BACK FACE TO AVOID LASING ACTION .
- ACTIVE LAYER IS HEAVILY DOPED (WITH Zn) TO REDUCE MINORITY CARRIER LIFE TIME & IMPROVE MODULATION BW.
- MODULATION BW OF 600 MHz IS POSSIBLE .

## HIGH SPEED In Ga As EDGE EMITTING LED'S

- 4  $\mu\text{w}$  to 6  $\mu\text{w}$  POWER CAN BE LAUNCHED AT *100 mA* AND 240 mA DRIVE CURRENT RESPECTIVELY INTO A SINGLE MODE FIBER.
- 7 $\mu\text{w}$  POWER IN BURIED HETROSTRUCTURE WITH 20 mA DRIVE CURRENT LAUNCHED INTO SM FIBER

# V-GROOVED SUBSTRATE BH ELED



V-grooved substrate BH ELED

## V-GROOVED SUBSTRATE BH ELED

FRONT FACE IS AR COATED

REAR FACE ETCHED SLANTLY TO SUPPRESS LASING

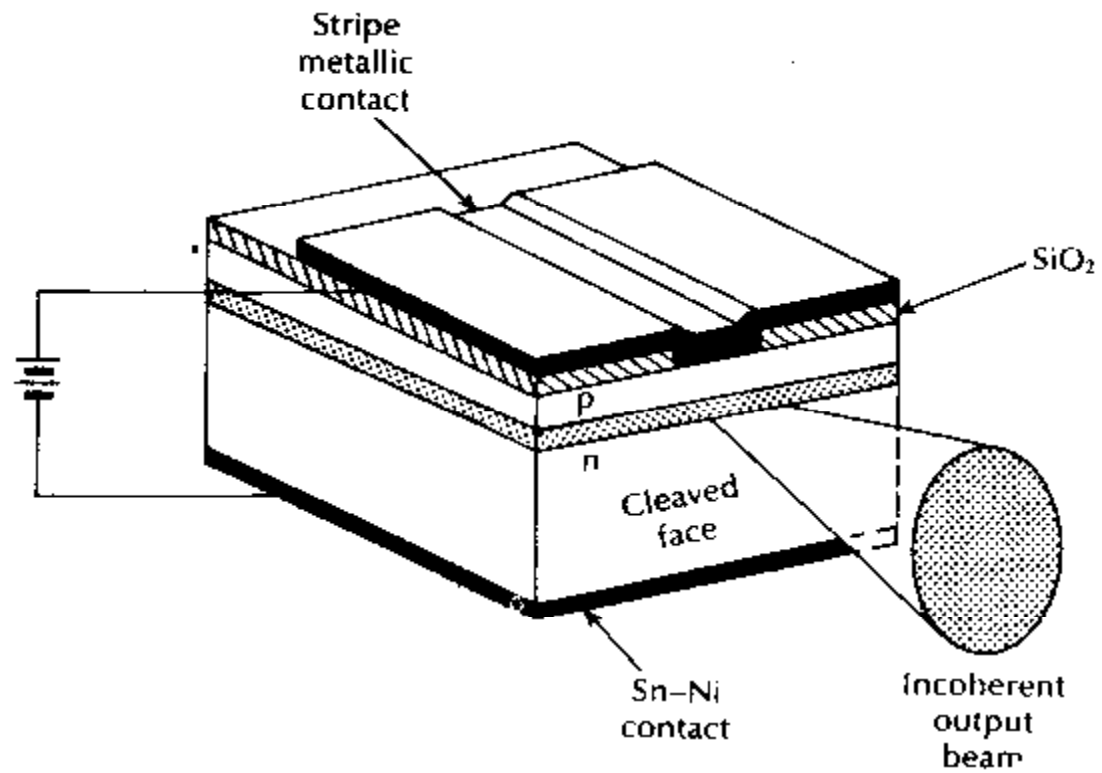
$\lambda \rightarrow 1.3 \mu\text{m}$ , 3dB Mod BW  $\approx 350$  MHz

**OPT. POWER  $\approx 30 \mu\text{W}$  (INTO SINGLE MODE FIBER)**

**BY LENS COUPLING, POWER UPTO  $200 \mu\text{w}$  CAN BE LAUNCHED  
WITH DRIVE CURRENT OF 100 mA.**

SPECTRAL WIDTH = 50 nm ( narrow )

## Al Ga As CONTACT STRIPE SLD



AlGaAs contact stripe SLD

## **Al Ga As CONTACT STRIPE SLD (contd)**

PROVIDES SIGNIFICANT BENEFITS OVER ELED & SLED

Advantages :

1. HIGH OUTPUT POWER
2. DIRECTIONAL BEAM
3. NARROW SPECTRAL LINE WIDTH
4. HIGHER MODULATION BW.



## Al Ga As CONTACT STRIPE SLD(contd)

- p- n JUNCTION IN THE FORM OF A LONG RECTANGULAR STRIPE .
- ONE END OF THE DEVICE IS MADE LOSSY IN A MANNER TO PREVENT REFLECTIONS (TO SUPPRESS LASING)
- .OUTPUT IS FROM THE OTHER END.DEVICE GIVES PEAK O/P POWER OF 60 mw AT 0.87  $\mu\text{m}$  WAVELENGTH
- ANTI REFLECTION COATING APPLICATION REDUCES LASER RESONANCE POSSIBILITY .

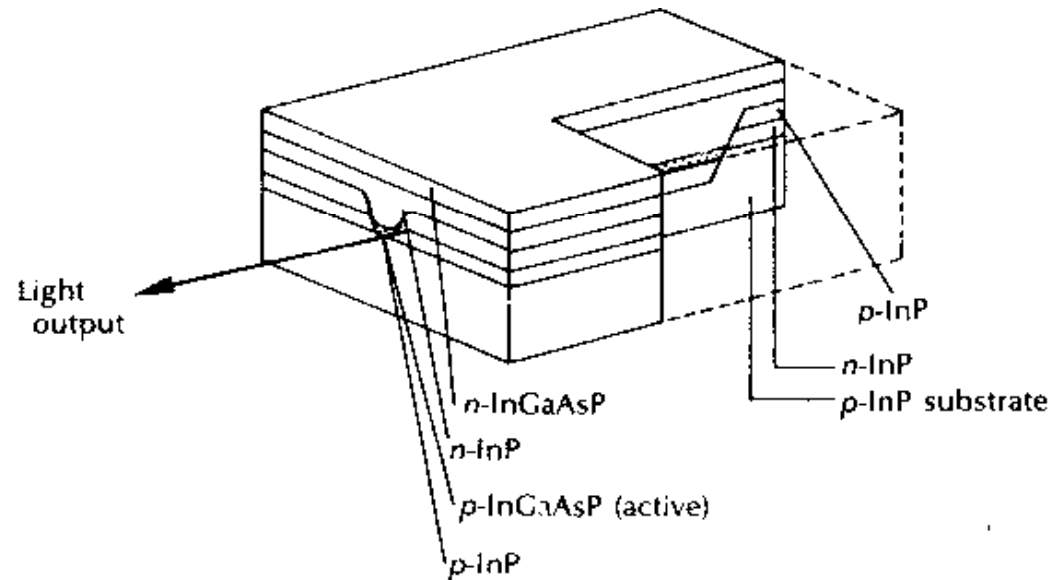
## Al Ga As CONTACT STRIPE SLD(contd)

- **DEVICE PARAMETERS**
- 550  $\mu\text{w}$  POWER – 50  $\mu\text{m}$  DIA MMGI FIBER-250 mA
- 250  $\mu\text{w}$  POWER – SINGLE MODE FIBER – 100 mA
- **LINEWIDTH** : 30 TO 40 nm COMPARED TO 60 TO 90 nm ASSOCIATED WITH CONVENTIONAL ELED'S

## InGaAsP / InP SLD

- STRUCTURE EMITS AT 1.3  $\mu\text{m}$
- BURRIED ACTIVE LAYER WITHIN V-SHAPED GROOVE ON p - TYPE InP SUBSTRATE.
- LOW LEAKAGE CURRENT
- A LIGHT DIFFUSION SURFACE IS PLACED WITHIN THE DEVICE WHICH SCATTERS THE BACKWARD LIGHT. THIS SCATTERING FROM THE ACTIVE LAYER DECREASES FEEDBACK INTO THIS LAYER
- AN AR COATING IS PROVIDED ON THE O/ P FACET.
- HIGH O / P POWER OF 1 mw CAN BE COUPLED INTO A SINGLE MODE FIBER.

## InGaAsP SLD / InP SLD



## High output power InGaAsP SLD

### **DRAWBACKS - SLD**

- HIGH DRIVE CURRENT
- NON – LINEAR O/P CHARACTERISTIC.
- INCREASED TEMP. DEPENDECE OF O/P POWER.

# LENS COUPLING TO FIBER

**COUPLING  $\eta = \frac{\text{POWER COUPLED (INTO THE FIBRE)}}{\text{TOTAL POWER EMITTED}}$**

COUPLING EFFICIENCY IS GENERALLY POOR (1 TO 2%)

USE OF LENSES IMPROVES THE COUPLING EFFICIENCY BY 2 TO 5 TIMES.

**FOR BETTER COUPLING FIBER CORE DIA  $\gg$  WIDTH OF EMISSION REGION.**