

A decorative graphic on the left side of the slide consists of light blue lines and circles, resembling a circuit board or network diagram. The lines are vertical and horizontal, with some branching out to small circles. The background is a gradient of blue, darker at the bottom and lighter at the top.

NETWORK THEORY



LECTURE 5

SECTION B

TOPIC COVERED :TWO PORT NETWORK

Properties of the S Matrix

❖ For **reciprocal** networks, the S -matrix is symmetric.

$$\Rightarrow [S] = [S]^T$$

Note:

$$\text{If } [A][B] = [U]$$

then

$$[B][A] = [U]$$

❖ For **lossless** networks, the S -matrix is unitary.

$$\Rightarrow [S]^T [S]^* = [S]^* [S]^T = [U]$$

Identity matrix

Equivalently,

$$[S]^{T*} = [S]^{-1}$$

Notation: $[S]^\dagger = [S]^H = [S]^{T*}$

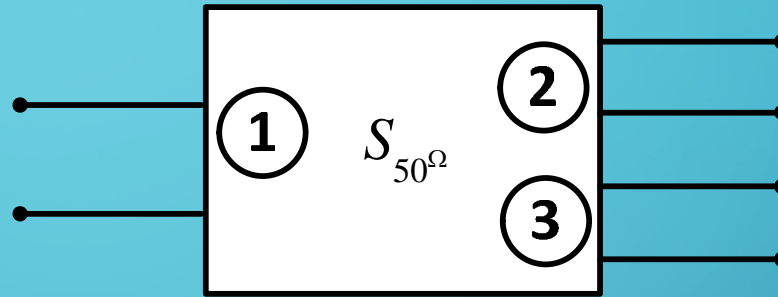
so $[S]^\dagger = [S]^{-1}$

N -port network

Take (i, j) element $\Rightarrow \sum_{k=1}^N S_{ik}^T S_{kj}^* = \sum_{k=1}^N S_{ki} S_{kj}^* = \delta_{ij} \quad \delta_{ij} = \begin{cases} 1; & i = j \\ 0; & i \neq j \end{cases}$

Example

$$[S_{50\Omega}] = \begin{bmatrix} 0 & \frac{-j}{\sqrt{2}} & \frac{-j}{\sqrt{2}} \\ \frac{-j}{\sqrt{2}} & 0 & 0 \\ \frac{-j}{\sqrt{2}} & 0 & 0 \end{bmatrix}$$



Not unitary → **Not lossless**

(For example, column 2 dotted with the conjugate of column three is not zero.)

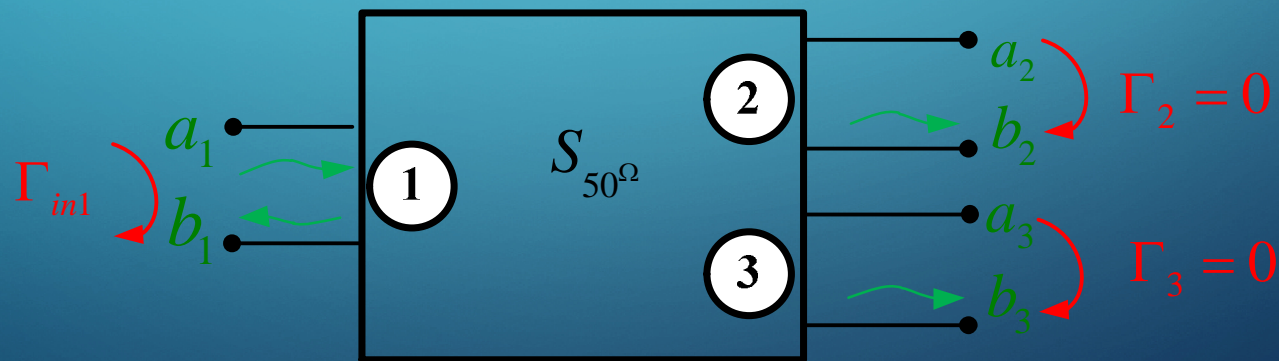
- 1) Find the input impedance looking into port 1 when ports 2 and 3 are terminated in $50 [\Omega]$ loads.
- 2) Find the input impedance looking into port 1 when port 2 is terminated in a $75 [\Omega]$ load and port 3 is terminated in a $50 [\Omega]$ load.

Example (cont.)

1 If ports 2 and 3 are terminated in $50 \text{ } [\Omega]$ ($a_2 = a_3 = 0$):

$$b_1 = S_{11}a_1 + S_{12}a_2 + S_{13}a_3$$

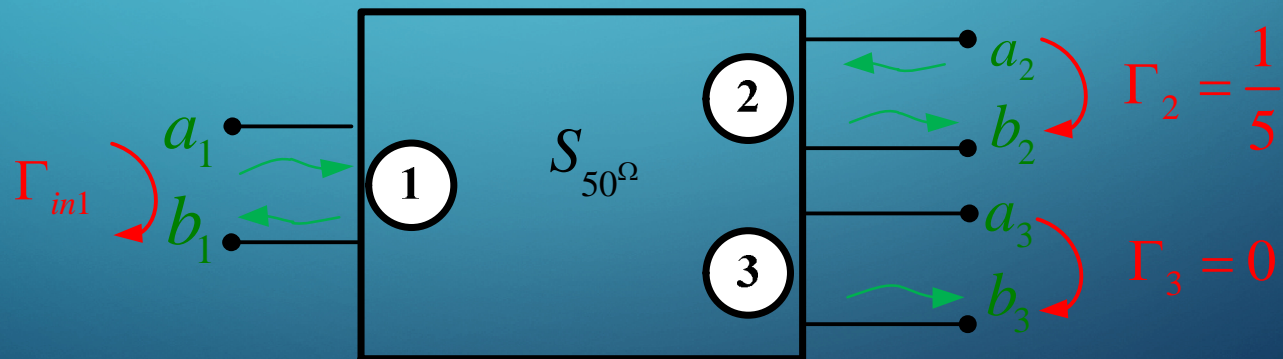
$$\Rightarrow \Gamma_{in1} = \frac{b_1}{a_1} = S_{11} = 0 \quad \Rightarrow \quad Z_{in1} = 50[\Omega]$$



Example (cont.)

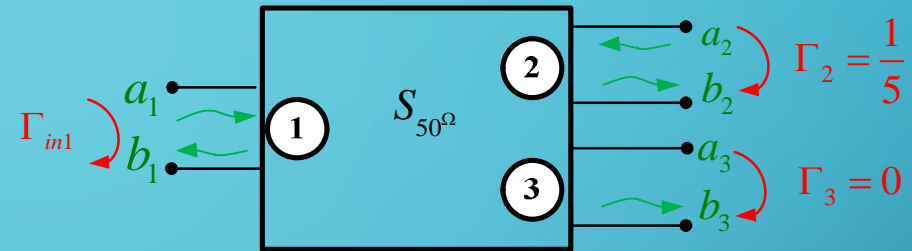
2) If port 2 is terminated in 75 [Ω] and port 3 in 50 [Ω]:

$$\Rightarrow \Gamma_2 = \frac{a_2}{b_2} = \frac{75 - 50}{75 + 50} = \frac{1}{5}$$



Example (cont.)

$$\begin{bmatrix} b_1 \\ b_2 \\ b_3 \end{bmatrix} = \begin{bmatrix} 0 & \frac{-j}{\sqrt{2}} & \frac{j}{\sqrt{2}} \\ \frac{-j}{\sqrt{2}} & 0 & 0 \\ \frac{-j}{\sqrt{2}} & 0 & 0 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$



$$\Rightarrow \Gamma_{in1} = \frac{b_1}{a_1} = \cancel{S_{11}} + S_{12} \frac{a_2}{a_1} + S_{13} \frac{a_3}{a_1}$$

$$b_2 / a_1 = \cancel{S_{21}} + S_{22} \left(\frac{a_2}{a_1} \right) + \cancel{S_{23}} \left(\frac{a_3}{a_1} \right)$$

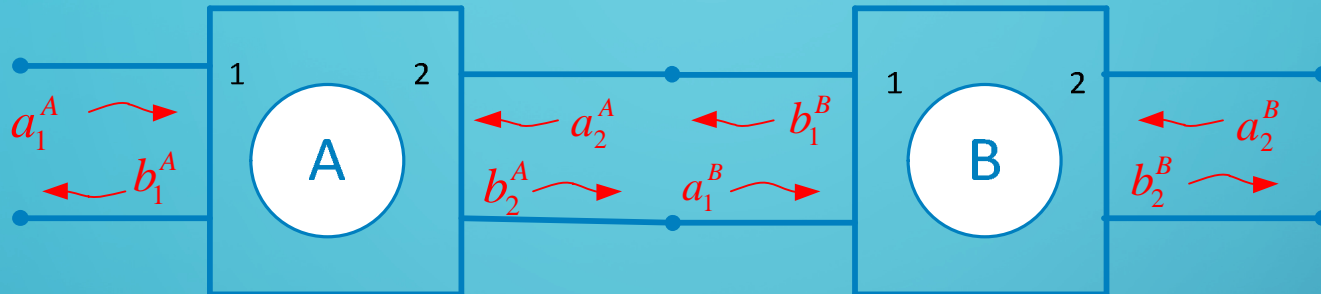
$$= S_{12} \left(\Gamma_2 \frac{b_2}{a_1} \right) = S_{12} (\Gamma_2 S_{21}) = \left(\frac{-j}{\sqrt{2}} \right) \left(\frac{1}{5} \right) \left(\frac{-j}{\sqrt{2}} \right) = -\frac{1}{10}$$

$$a_2 = \Gamma_2 b_2$$

$$\Rightarrow Z_{in1} = 50 \left(\frac{1 + \Gamma_{in1}}{1 - \Gamma_{in1}} \right) = 44.55 [\Omega]$$

Transfer (T) Matrix

For cascaded 2-port networks:



T Matrix:

$$\begin{bmatrix} a_1 \\ b_1 \end{bmatrix} = \begin{bmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{bmatrix} \begin{bmatrix} b_2 \\ a_2 \end{bmatrix}$$

$$= [T] \begin{bmatrix} b_2 \\ a_2 \end{bmatrix}$$

$$[T] = \begin{bmatrix} 1 & -S_{22} \\ S_{21} & S_{21} \\ S_{11} & S_{12} - \frac{S_{11}S_{22}}{S_{21}} \\ S_{21} & \end{bmatrix}$$

$$[S] = \begin{bmatrix} -\frac{T_{21}}{T_{22}} & \frac{1}{T_{22}} \\ T_{11} - \frac{T_{12}^2}{T_{22}} & \frac{T_{12}}{T_{22}} \end{bmatrix}$$

(Derivation omitted)

Transfer (T) Matrix (cont.)

$$\Rightarrow \begin{bmatrix} a_1^A \\ b_1^A \end{bmatrix} = [T^A] \begin{bmatrix} b_2^A \\ a_2^A \end{bmatrix}$$

But $\begin{bmatrix} b_2^A \\ a_2^A \end{bmatrix} = \begin{bmatrix} a_1^B \\ b_1^B \end{bmatrix}$

$$\Rightarrow \begin{bmatrix} a_1^A \\ b_1^A \end{bmatrix} = [T^A] \begin{bmatrix} a_1^B \\ b_1^B \end{bmatrix}$$

Hence $\begin{bmatrix} a_1^A \\ b_1^A \end{bmatrix} = \underbrace{[T^A][T^B]}_{[T^{AB}]} \begin{bmatrix} b_2^B \\ a_2^B \end{bmatrix}$

The T matrix of a cascaded set of networks is the product of the T matrices.

Conversion Between Parameters

TABLE 4.2 Conversions Between Two-Port Network Parameters

	S	Z	Y	ABCD
S_{11}	S_{11}	$\frac{(Z_{11} - Z_0)(Z_{22} + Z_0) - Z_{12}Z_{21}}{\Delta Z}$	$\frac{(Y_0 - Y_{11})(Y_0 + Y_{22}) + Y_{12}Y_{21}}{\Delta Y}$	$\frac{A + B/Z_0 - CZ_0 - D}{A + B/Z_0 + CZ_0 + D}$
S_{12}	S_{12}	$\frac{2Z_{12}Z_0}{\Delta Z}$	$\frac{-2Y_{12}Y_0}{\Delta Y}$	$\frac{2(AD - BC)}{A + B/Z_0 + CZ_0 + D}$
S_{21}	S_{21}	$\frac{2Z_{21}Z_0}{\Delta Z}$	$\frac{-2Y_{21}Y_0}{\Delta Y}$	$\frac{2}{A + B/Z_0 + CZ_0 + D}$
S_{22}	S_{22}	$\frac{(Z_{11} + Z_0)(Z_{22} - Z_0) - Z_{12}Z_{21}}{\Delta Z}$	$\frac{(Y_0 + Y_{11})(Y_0 - Y_{22}) + Y_{12}Y_{21}}{\Delta Y}$	$\frac{-A + B/Z_0 - CZ_0 + D}{A + B/Z_0 + CZ_0 + D}$
Z_{11}	$Z_0 \frac{(1 + S_{11})(1 - S_{22}) + S_{12}S_{21}}{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}$	Z_{11}	$\frac{Y_{22}}{ Y }$	$\frac{A}{C}$
Z_{12}	$Z_0 \frac{2S_{12}}{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}$	Z_{12}	$\frac{-Y_{12}}{ Y }$	$\frac{AD - BC}{C}$
Z_{21}	$Z_0 \frac{2S_{21}}{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}$	Z_{21}	$\frac{-Y_{21}}{ Y }$	$\frac{1}{C}$
Z_{22}	$Z_0 \frac{(1 - S_{11})(1 + S_{22}) + S_{12}S_{21}}{(1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}$	Z_{22}	$\frac{Y_{11}}{ Y }$	$\frac{D}{C}$
Y_{11}	$Y_0 \frac{(1 - S_{11})(1 + S_{22}) + S_{12}S_{21}}{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}$	$\frac{Z_{22}}{ Z }$	Y_{11}	$\frac{D}{B}$
Y_{12}	$Y_0 \frac{-2S_{12}}{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}$	$\frac{-Z_{12}}{ Z }$	Y_{12}	$\frac{BC - AD}{B}$
Y_{21}	$Y_0 \frac{-2S_{21}}{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}$	$\frac{-Z_{21}}{ Z }$	Y_{21}	$\frac{-1}{B}$
Y_{22}	$Y_0 \frac{(1 + S_{11})(1 - S_{22}) + S_{12}S_{21}}{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}$	$\frac{Z_{11}}{ Z }$	Y_{22}	$\frac{A}{B}$
A	$\frac{(1 + S_{11})(1 - S_{22}) + S_{12}S_{21}}{2S_{21}}$	$\frac{Z_{11}}{Z_{21}}$	$\frac{-Y_{22}}{Y_{21}}$	A
B	$Z_0 \frac{(1 + S_{11})(1 + S_{22}) - S_{12}S_{21}}{2S_{21}}$	$\frac{ Z }{Z_{21}}$	$\frac{-1}{Y_{21}}$	B
C	$\frac{1 - (1 - S_{11})(1 - S_{22}) - S_{12}S_{21}}{2S_{21}}$	$\frac{1}{Z_{21}}$	$\frac{- Y }{Y_{21}}$	C
D	$\frac{(1 - S_{11})(1 + S_{22}) + S_{12}S_{21}}{2S_{21}}$	$\frac{Z_{22}}{Z_{21}}$	$\frac{-Y_{11}}{Y_{21}}$	D

$$|Z| = Z_{11}Z_{22} - Z_{12}Z_{21}$$

$$|Y| = Y_{11}Y_{22} - Y_{12}Y_{21}$$

$$\Delta Y = (Y_{11} + Y_0)(Y_{22} + Y_0) - Y_{12}Y_{21}$$

$$\Delta Z = (Z_{11} + Z_0)(Z_{22} + Z_0) - Z_{12}Z_{21}$$

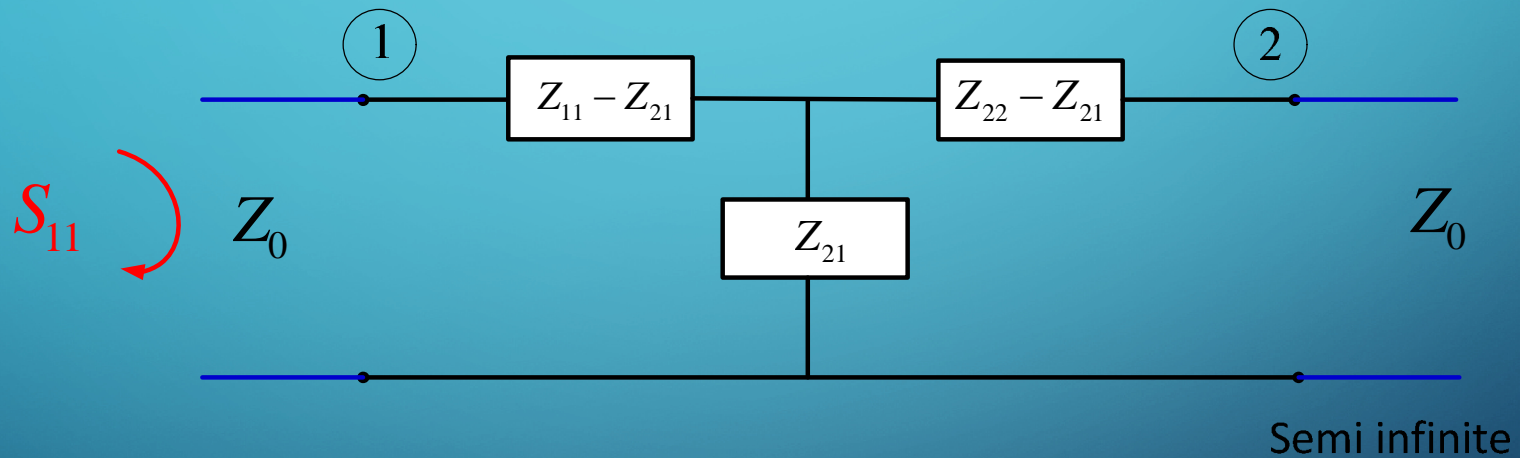
$$Y_0 = 1/Z_0$$

Example

Derive S_{ij} from the Z parameters.

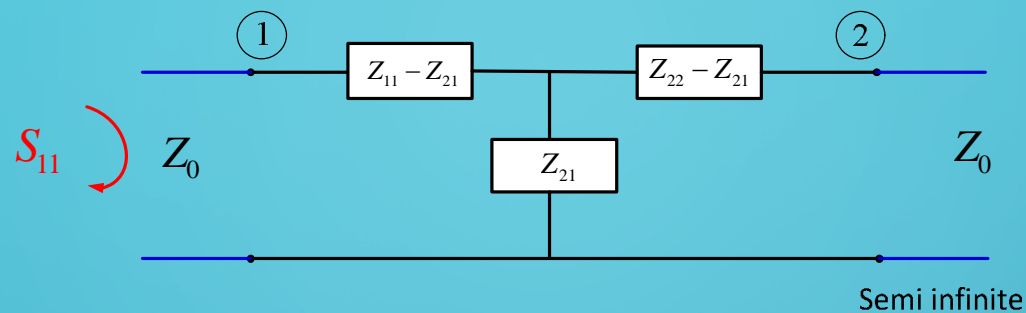
(The result is given inside row 1, column 2, of the previous table.)

S_{11} Calculation:



$$S_{11} = \Gamma_{in1} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \quad Z_{in} = (Z_{11} - Z_{21}) + (Z_{21}) \parallel [(Z_{22} - Z_{21}) + Z_0]$$

Example (cont.)



$$Z_{in} = (Z_{11} - Z_{21}) + (Z_{21}) \parallel [(Z_{22} - Z_{21}) + Z_0]$$

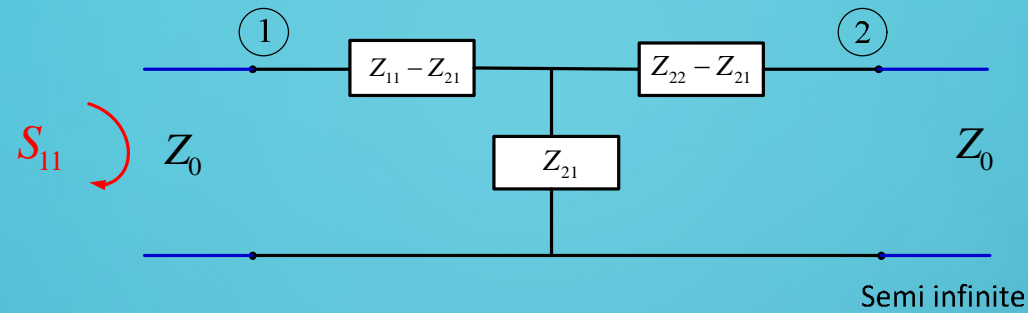
$$= (Z_{11} - Z_{21}) + \frac{Z_{21}(Z_{22} + Z_0 - Z_{21})}{Z_{22} + Z_0}$$

$$= \frac{(Z_{11} - Z_{21})(Z_{22} + Z_0) + Z_{21}(Z_{22} + Z_0 - Z_{21})}{Z_{22} + Z_0}$$

$$= \frac{Z_{11}Z_{22} + Z_{11}Z_0 - Z_{21}Z_{22} - Z_{21}Z_0 + Z_{21}Z_{22} + Z_{21}Z_0 - Z_{21}^2}{Z_{22} + Z_0}$$

$$= \frac{Z_{11}Z_{22} + Z_{11}Z_0 - Z_{21}^2}{Z_{22} + Z_0}$$

Example (cont.)



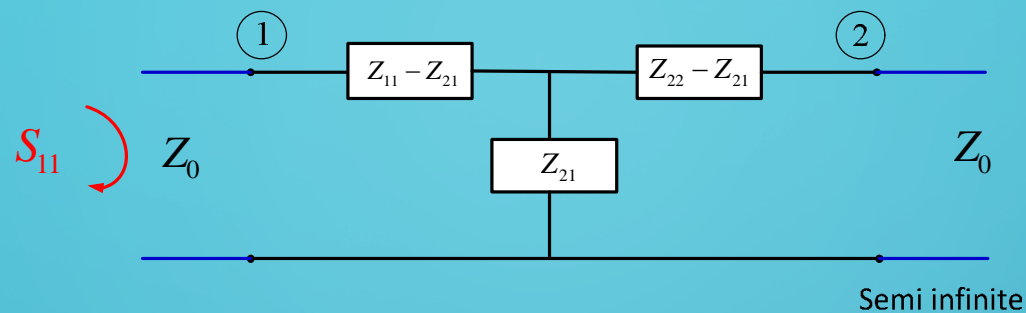
$$Z_{in} = \frac{Z_{11}(Z_0 + Z_{22}) - Z_{21}^2}{Z_{22} + Z_0}$$

$$S_{11} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0}$$

so

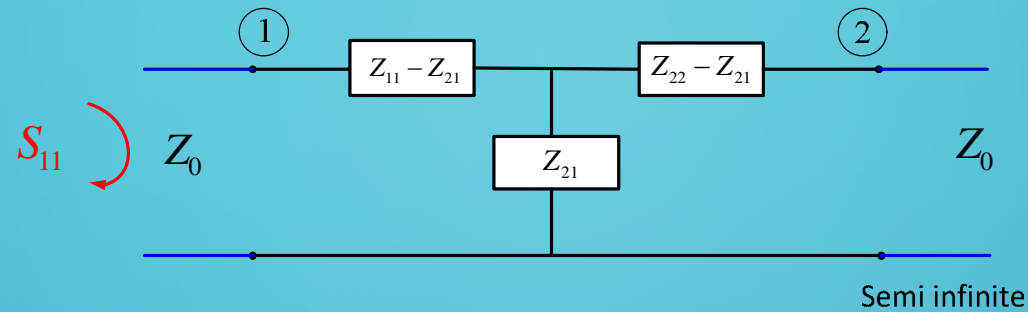
$$S_{11} = \frac{Z_{11}(Z_0 + Z_{22}) - Z_{21}^2 - Z_0(Z_0 + Z_{22})}{Z_{11}(Z_0 + Z_{22}) - Z_{21}^2 + Z_0(Z_0 + Z_{22})}$$

Example (cont.)



$$\begin{aligned}
 S_{11} &= \frac{Z_{11}(Z_0 + Z_{22}) - Z_{21}^2 - Z_0(Z_0 + Z_{22})}{Z_{11}(Z_0 + Z_{22}) - Z_{21}^2 + Z_0(Z_0 + Z_{22})} \\
 &= \frac{Z_{11}Z_0 + Z_{11}Z_{22} - Z_{21}^2 - Z_0^2 - Z_0Z_{22}}{Z_{11}Z_0 + Z_{11}Z_{22} - Z_{21}^2 + Z_0^2 + Z_0Z_{22}} \\
 &= \frac{(Z_0 + Z_{22})(Z_{11} - Z_0) - Z_{21}^2}{(Z_0 + Z_{22})(Z_{11} + Z_0) - Z_{21}^2}
 \end{aligned}$$

Example (cont.)



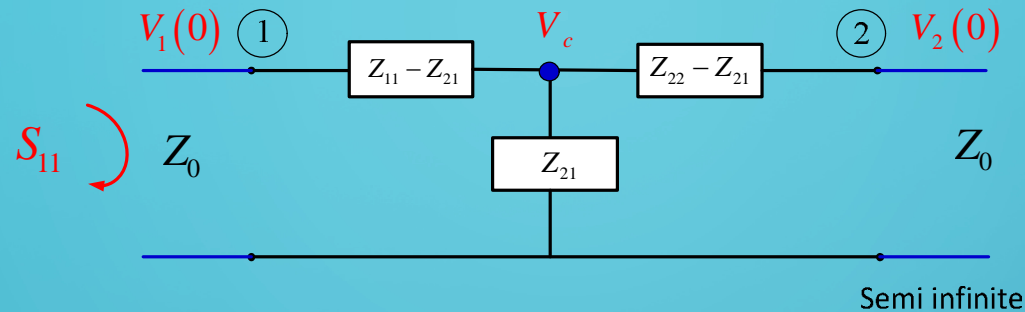
$$S_{11} = \frac{(Z_0 + Z_{22})(Z_{11} - Z_0) - Z_{21}^2}{(Z_0 + Z_{22})(Z_{11} + Z_0) - Z_{21}^2}$$

Note: to get S_{22} , simply let $Z_{11} \rightarrow Z_{22}$ in the previous result.

$$S_{22} = \frac{(Z_0 + Z_{11})(Z_{22} - Z_0) - Z_{21}^2}{(Z_0 + Z_{11})(Z_{22} + Z_0) - Z_{21}^2}$$

Example (cont.)

S_{21} Calculation:



Assume $V_1^+(0) = 1$ [V]

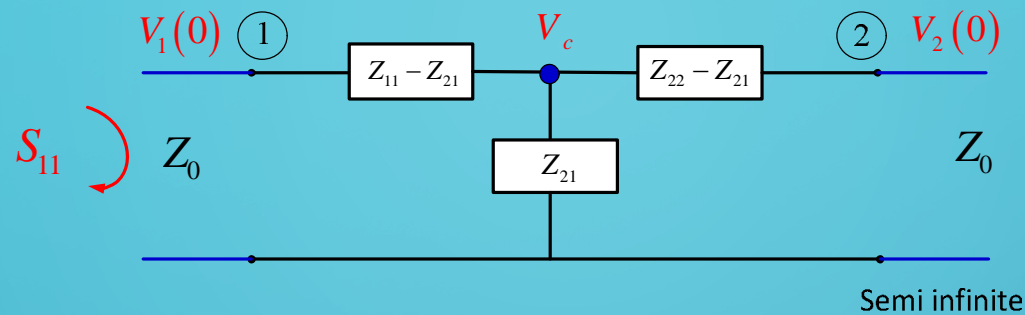
$$V_1(0) = 1 + S_{11} \quad S_{21} = V_2^-(0) = V_2(0)$$

Use voltage divider equation twice:

$$V_c = V_1(0) \left(\frac{(Z_{21}) \parallel [(Z_{22} - Z_{21}) + Z_0]}{(Z_{11} - Z_{21}) + (Z_{21}) \parallel [(Z_{22} - Z_{21}) + Z_0]} \right)$$

$$V_2(0) = V_c \left(\frac{Z_0}{(Z_{22} - Z_{21}) + Z_0} \right)$$

Example (cont.)



Hence

$$S_{21} = (1 + S_{11}) \left(\frac{(Z_{21}) \parallel [(Z_{22} - Z_{21}) + Z_0]}{(Z_{11} - Z_{21}) + (Z_{21}) \parallel [(Z_{22} - Z_{21}) + Z_0]} \right) \left(\frac{Z_0}{(Z_{22} - Z_{21}) + Z_0} \right)$$

After simplifying, we should get the result in the table.

(You are welcome to check it!)