

A decorative graphic on the left side of the slide, consisting of white lines and circles that resemble a circuit board or network diagram. The lines are vertical and horizontal, with some diagonal connections, and the circles are small and white, placed at various points along the lines.

NETWORK THEORY



LECTURE 3

SECTION B

TOPIC COVERED :TWO PORT NETWORK

Reciprocal Networks

If a network does not contain non-reciprocal devices or materials* (i.e. ferrites, or active devices), then the network is “reciprocal.”

$$\Rightarrow Z_{ij} = Z_{ji} \quad (Y_{ij} = Y_{ji})$$

Note: The inverse of a symmetric matrix is symmetric.

$$\Rightarrow [Z] \text{ and } [Y] \text{ are symmetric}$$

* A reciprocal material is one that has reciprocal permittivity and permeability tensors. A reciprocal device is one that is made from reciprocal materials

Example of a nonreciprocal material: a biased ferrite

(This is very useful for making isolators and circulators.)

Reciprocal Materials

$$\underline{D} = \underline{\underline{\epsilon}} \cdot \underline{E}$$

$$\underline{B} = \underline{\underline{\mu}} \cdot \underline{H}$$

$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \begin{bmatrix} \epsilon_{xx} & \epsilon_{xy} & \epsilon_{xz} \\ \epsilon_{yx} & \epsilon_{yy} & \epsilon_{yz} \\ \epsilon_{zx} & \epsilon_{zy} & \epsilon_{zz} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} \quad \begin{bmatrix} B_x \\ B_y \\ B_z \end{bmatrix} = \begin{bmatrix} \mu_{xx} & \mu_{xy} & \mu_{xz} \\ \mu_{yx} & \mu_{yy} & \mu_{yz} \\ \mu_{zx} & \mu_{zy} & \mu_{zz} \end{bmatrix} \begin{bmatrix} \mu_x \\ \mu_y \\ \mu_z \end{bmatrix}$$

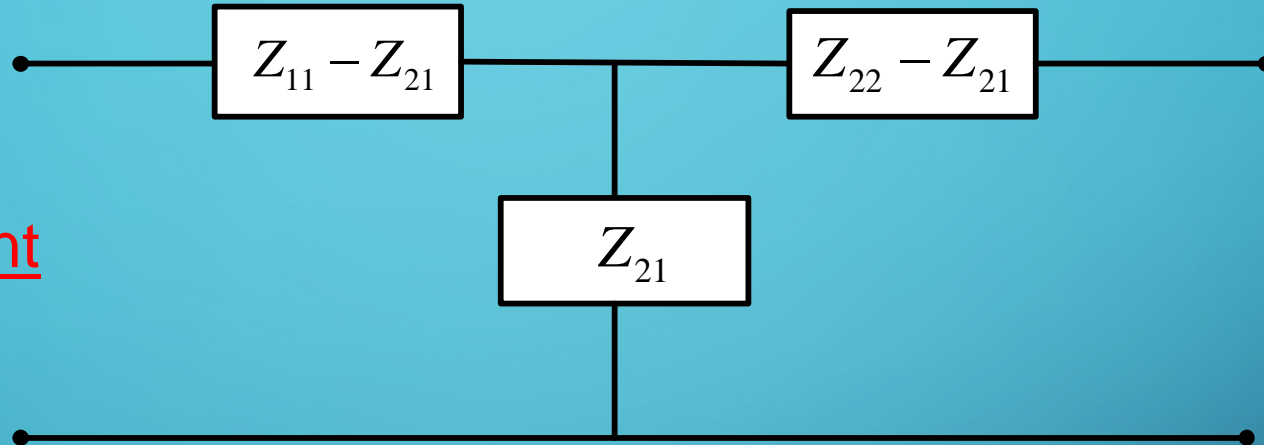
Reciprocal: $\epsilon_{ij} = \epsilon_{ji}$, $\mu_{ij} = \mu_{ji}$

Ferrite: $\underline{\underline{\mu}} = \mu_0 \begin{bmatrix} \alpha & j\gamma & 0 \\ -j\gamma & \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$ $\underline{\underline{\mu}}$ is not symmetric!

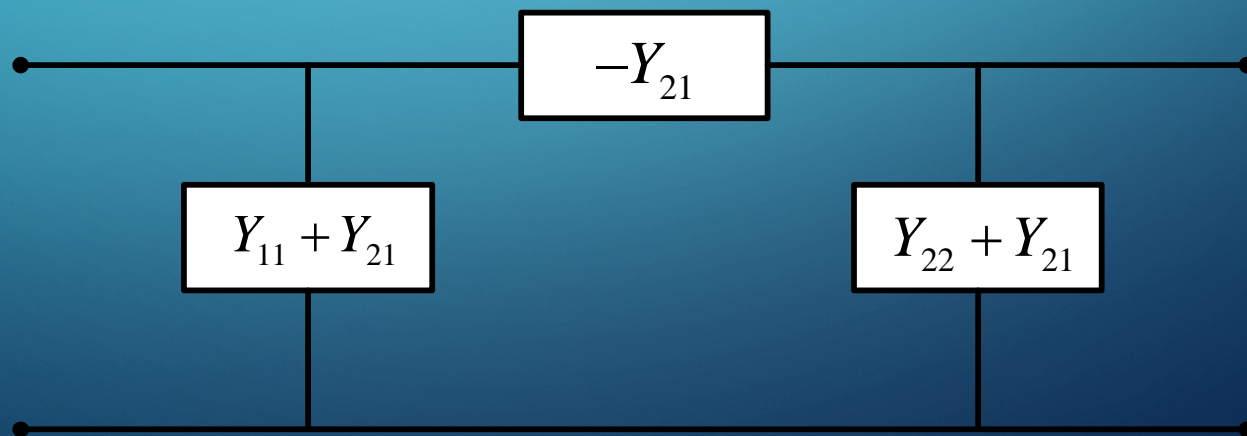
Reciprocal Networks (cont.)

We can show that the equivalent circuits for reciprocal 2-port networks are:

T-equivalent



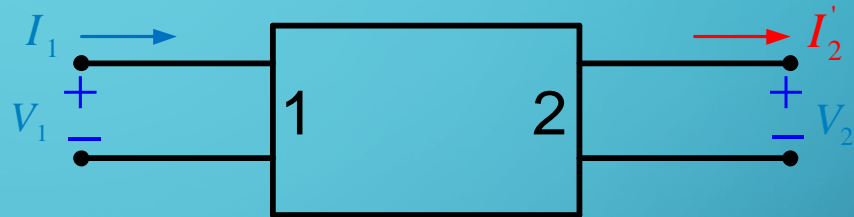
Pi-
equivalent



ABCD-Parameters

They are defined only for 2-port networks.

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ I_2' \end{bmatrix}$$



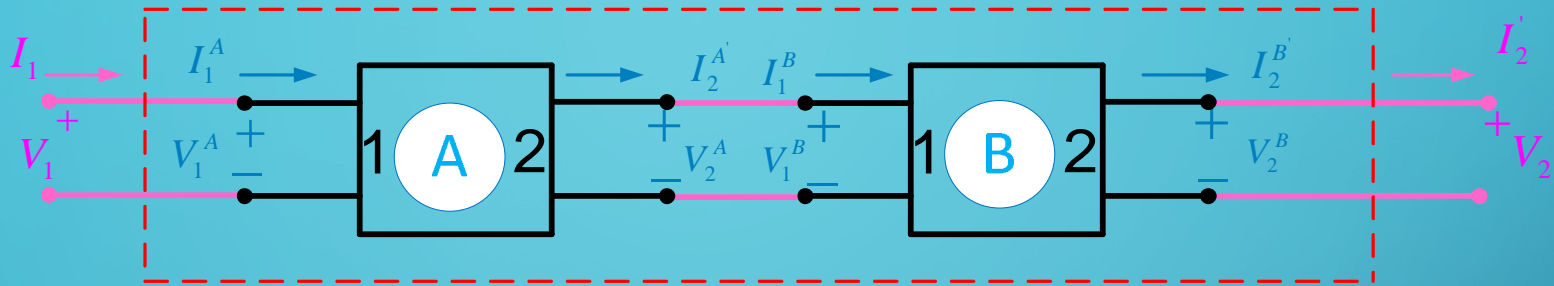
$$A = \left. \frac{V_1}{V_2} \right|_{I_2' = 0}$$

$$C = \left. \frac{I_1}{V_2} \right|_{I_2' = 0}$$

$$B = \left. \frac{V_1}{I_2'} \right|_{V_2 = 0}$$

$$D = \left. \frac{I_1}{I_2'} \right|_{V_2 = 0}$$

Cascaded Networks



$$\begin{aligned} \begin{bmatrix} V_1 \\ I_1 \end{bmatrix} &= \begin{bmatrix} V_1^A \\ I_1^A \end{bmatrix} = \begin{bmatrix} ABCD^A \end{bmatrix} \begin{bmatrix} V_2^A \\ I_2^A \end{bmatrix} \\ &= \begin{bmatrix} ABCD^A \end{bmatrix} \begin{bmatrix} V_1^B \\ I_1^B \end{bmatrix} \\ &= \underbrace{\begin{bmatrix} ABCD^A \end{bmatrix} \begin{bmatrix} ABCD^B \end{bmatrix}} \begin{bmatrix} V_2^B \\ I_2^B \end{bmatrix} \end{aligned}$$

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} ABCD^{AB} \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$

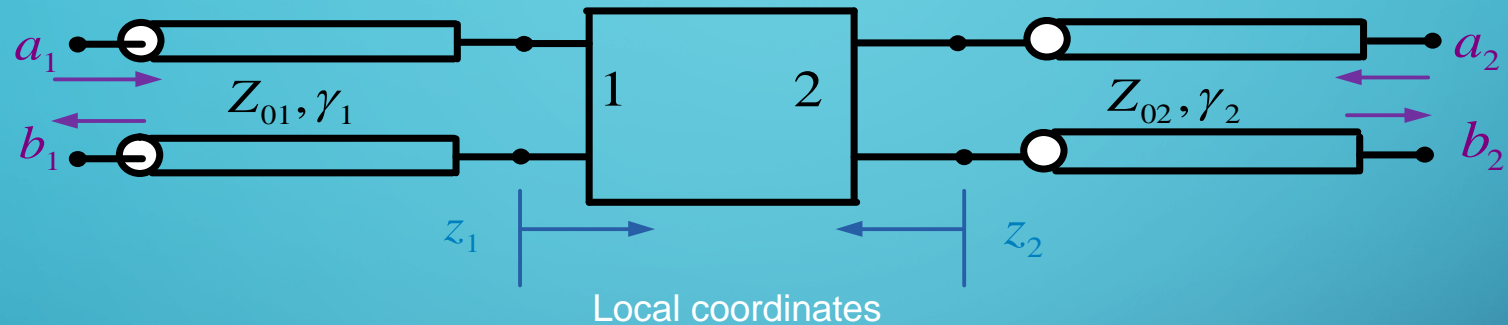
A nice property of the ABCD matrix is that it is easy to use with cascaded networks: you simply multiply the ABCD matrices together.

Scattering Parameters

- At high frequencies, Z , Y , h & ABCD parameters are difficult (if not impossible) to measure.
 - V and I are not uniquely defined
 - Even if defined, V and I are extremely difficult to measure (particularly I).
 - Required open and short-circuit conditions are often difficult to achieve.
- Scattering (S) parameters are often the best representation for multi-port networks at high frequency.

Scattering Parameters (cont.)

S -parameters are defined assuming transmission lines are connected to each port.



On each transmission line:

$$V_i(z_i) = V_{i0}^+ e^{-\gamma_i z_i} + V_{i0}^- e^{+\gamma_i z_i} = V_i^+(z_i) + V_i^-(z_i)$$

$$I_i(z_i) = \frac{V_i^+(z_i)}{Z_{0i}} - \frac{V_i^-(z_i)}{Z_{0i}} \quad i = 1, 2$$

$$\text{Incoming wave function} \equiv a_i(z_i) \equiv V_i^+(z_i) / \sqrt{Z_{0i}}$$

$$\text{Outgoing wave function} \equiv b_i(z_i) \equiv V_i^-(z_i) / \sqrt{Z_{0i}}$$

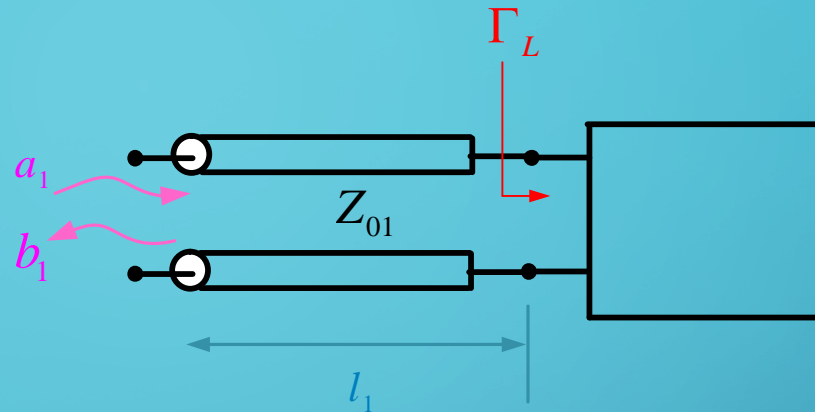
For a One-Port Network

$$\Gamma_L = \frac{V_1^-(0) / \sqrt{Z_{01}}}{V_1^+(0) / \sqrt{Z_{01}}}$$

$$= \frac{b_1(0)}{a_1(0)}$$

$$= S_{11}$$

$$\Rightarrow b_1(0) = \Gamma_L a_1(0) \\ = S_{11} a_1(0)$$

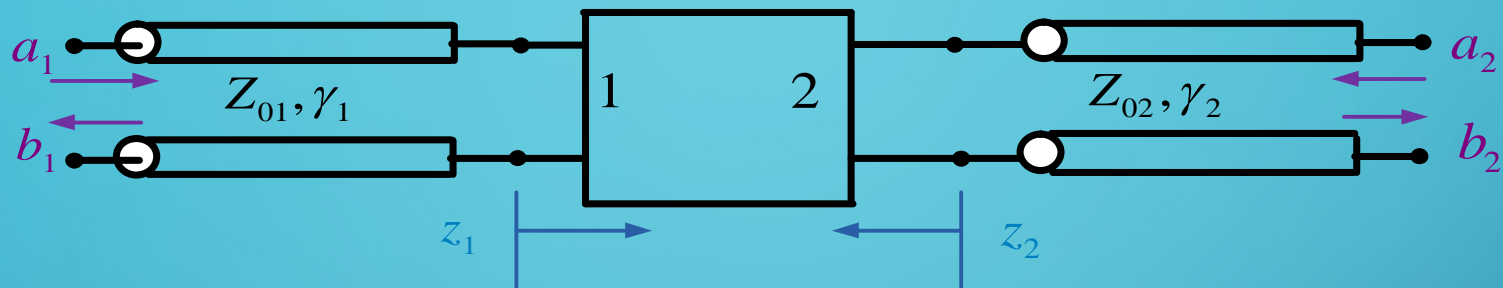


For a one-port network, S_{11} is defined to be the same as Γ_L .

Incoming wave function $\equiv a_i(z_i) \equiv V_i^+(z_i) / \sqrt{Z_{0i}}$

Outgoing wave function $\equiv b_i(z_i) \equiv V_i^-(z_i) / \sqrt{Z_{0i}}$

For a Two-Port Network



$$b_1(0) = S_{11}a_1(0) + S_{12}a_2(0)$$

$$b_2(0) = S_{21}a_1(0) + S_{22}a_2(0)$$

Scattering
matrix

$$\Rightarrow \begin{bmatrix} b_1(0) \\ b_2(0) \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \begin{bmatrix} a_1(0) \\ a_2(0) \end{bmatrix} \Rightarrow [b] = [S][a]$$