

A decorative graphic on the left side of the slide, consisting of white lines and circles that resemble a circuit board or network diagram. The lines are vertical and horizontal, with some diagonal connections, and the circles are small and white, placed at various points along the lines.

NETWORK THEORY



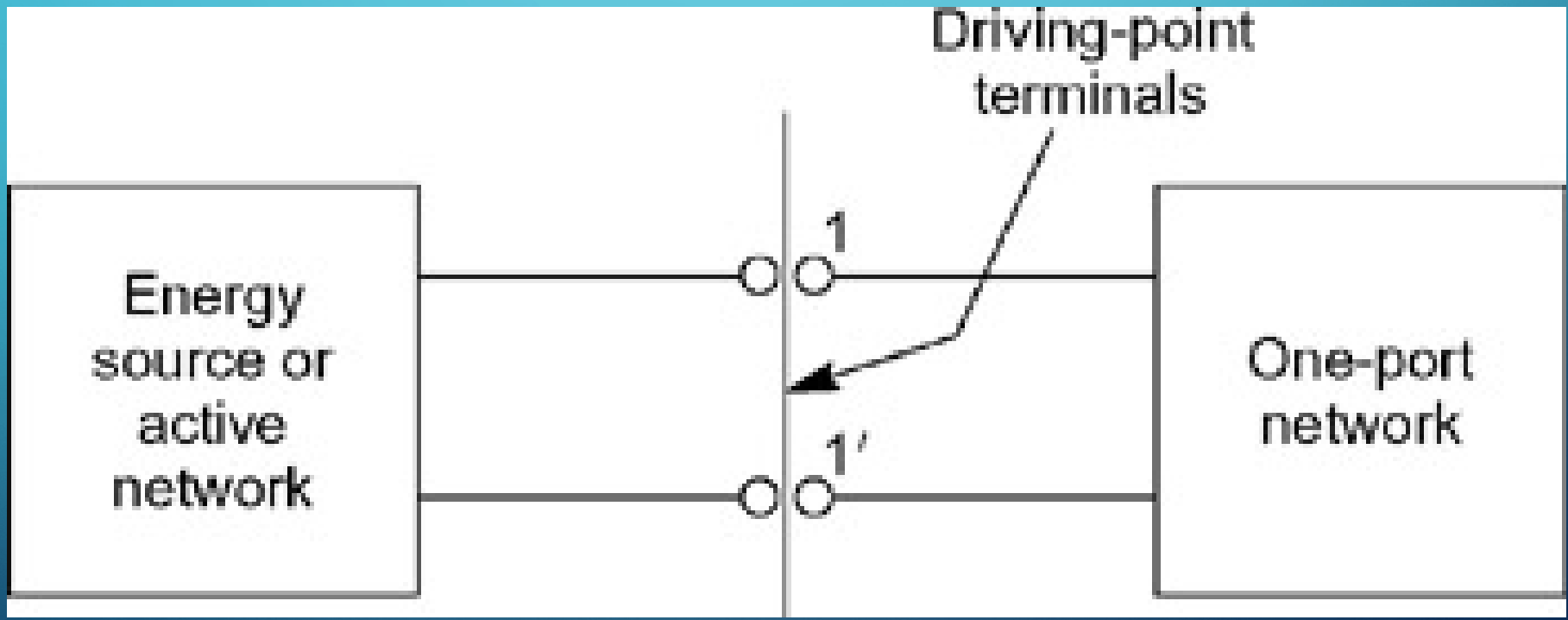
LECTURE 1

SECTION B

TOPIC COVERED: TERMINAL PAIRS OR PORTS

TERMINAL PAIRS OR PORTS

- Any network may be represented schematically by a rectangle or box as shown in Figure 1. A network may be used for a variety of purposes. Thus consider its use as a load connected to some other network. In order to connect it to the active network, there must be available two terminals of this passive network. Figure 1 shows a network with one pair of terminals 1-1 ? or with one port. Such a network may be called a *one-port network* or *one terminal-pair network*. When such a one-port network is connected to an energy source or an active network at its pair of terminals, the energy source provides the driving force for this one-port network and the pair of terminals constitute the *driving-point* of the network. One pair of terminals is known as a port.



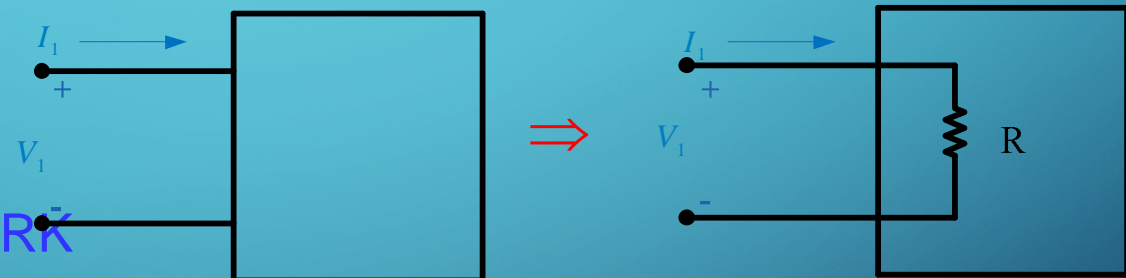
MULTI-PORT NETWORKS

A GENERAL CIRCUIT CAN BE REPRESENTED BY A MULTI-PORT NETWORK, WHERE THE “PORTS” ARE DEFINED AS ACCESS TERMINALS AT WHICH WE CAN DEFINE VOLTAGES AND CURRENTS.

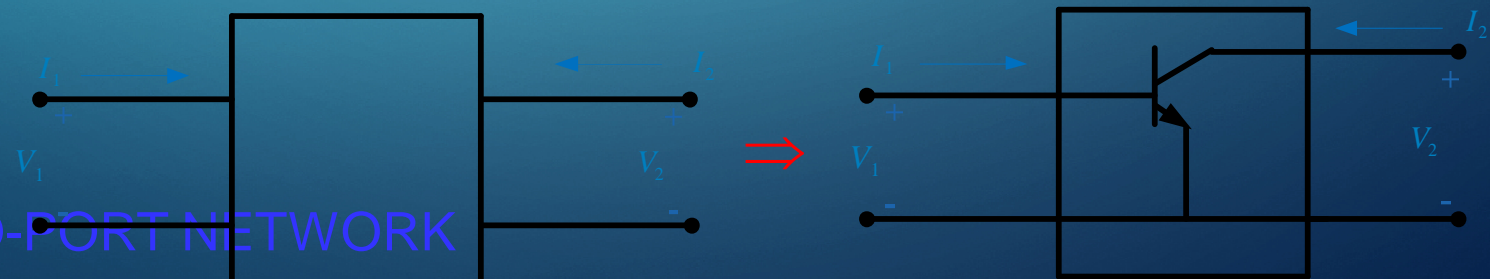
Note: Equal and opposite currents are assumed on the two wires of a port.

EXAMPLES:

1) ONE-PORT NETWORK



2) TWO-PORT NETWORK



Multiport Networks (cont.)

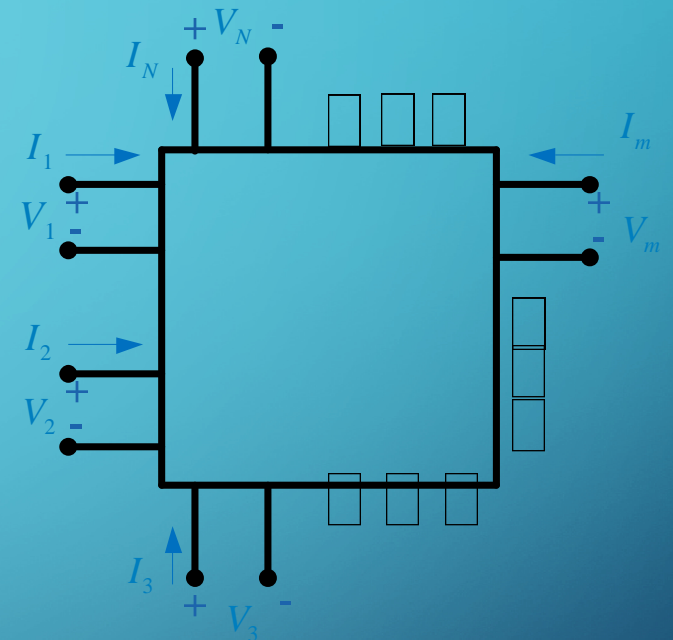
3) N -port Network

To represent multi-port networks we use:

- Z (impedance) parameters
- Y (admittance) parameters
- h (hybrid) parameters
- $ABCD$ parameters
- S (scattering) parameters

Not easily measurable at high frequency

Measurable at high frequency



Poynting Theorem (Phasor Domain)

$$\int_V -\frac{1}{2}(\underline{E} \cdot \underline{J}^{i*}) dV = \oint_S \underline{S} \cdot \underline{\hat{n}} dS$$
$$+ \int_V \left(\frac{1}{2} \omega \epsilon_c'' |\underline{E}|^2 + \frac{1}{2} \omega \mu'' |\underline{H}|^2 \right) dV$$
$$+ 2j\omega \int_V \left(\frac{1}{4} \mu' |\underline{H}|^2 - \frac{1}{4} \epsilon_c' |\underline{E}|^2 \right) dV$$



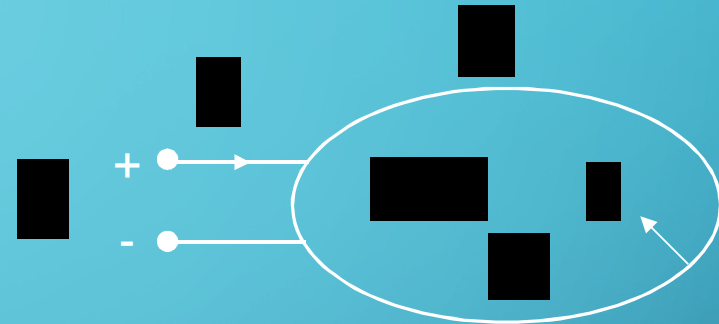
The last term is the
VARS consumed by
the region.

The notation $\langle \rangle$
denotes time-average.

$$P_s = P_f + \langle P_d \rangle + j(2\omega) (\langle W_m \rangle - \langle W_e \rangle)$$

Self Impedance

Consider a general **one-port** network



Complex power delivered to network:

$$P_{in} = \frac{1}{2} \oint_S (\underline{E} \times \underline{H}) \cdot \underline{\hat{n}} \, ds = P_d + j2\omega(W_m - W_e)$$

$$= \frac{1}{2} V_1 I_1^*$$

Average power dissipated in [W]
 $P_d = \langle P_d \rangle$

Average electric energy (in [J]) stored inside V

$$W_e = \langle W_e \rangle$$

Average magnetic energy (in [J]) stored inside V

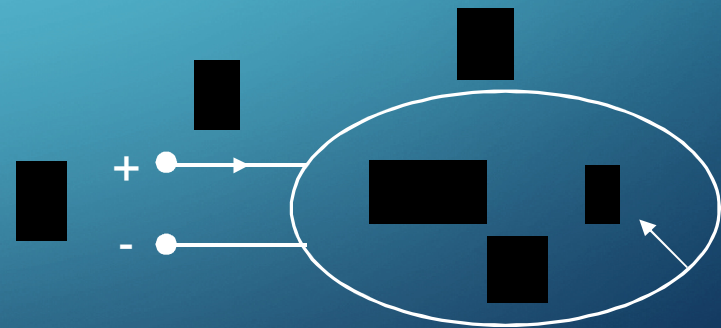
$$W_m = \langle W_m \rangle$$

Define Self Impedance (Z_{in})

$$Z_{in} \equiv \frac{V_1}{I_1} = \frac{V_1 I_1^*}{|I_1|^2} = \frac{\frac{1}{2} V_1 I_1^*}{\frac{1}{2} |I_1|^2} = \frac{P_{in}}{\frac{1}{2} |I_1|^2}$$
$$= R_{in} + jX_{in} = \frac{P_d + j2\omega(W_m - W_e)}{\frac{1}{2} |I_1|^2}$$

$$R_{in} = \frac{2P_d}{|I_1|^2}$$

$$X_{in} = \frac{4\omega(W_m - W_e)}{|I_1|^2}$$



Self Impedance (cont.)

We can show that for physically realizable networks the following apply:

$$V_1(-\omega) = V_1^*(\omega)$$

$$\Rightarrow Z_{in}(-\omega) = Z_{in}^*(\omega)$$

$$I_1(-\omega) = I_1^*(\omega)$$

$\Rightarrow R_{in}(\omega)$ is an even function of ω

$$Z_{in}(\omega) = R_{in}(\omega) + jX_{in}(\omega)$$

$X_{in}(\omega)$ is an odd function of ω

Note: Frequency is usually defined as a positive quantity. However, we consider the analytic continuation of the functions into the complex frequency plane.